STORMWATER REPORT

190 WASHINGTON STREET RE-DEVELOPMENT

WESTWOOD, MASSACHUSETTS

<u>Prepared For:</u> SKYE REALTY MANAGEMENT, LLC

> <u>Prepared By:</u> Marchionda & Associates, LP

> > April 12, 2023

190 WASHINGTON STREET STORMWATER REPORT

APRIL 12, 2023

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STORMWATER REPORT NARRATIVE

190 WASHINGTON STREET RE-DEVELOPMENT

April 12, 2023

Introduction:

Marchionda & Associates, L.P. has completed a storm water analysis for the redevelopment project proposed at 190 Washington Street in Westwood, Massachusetts. The purpose of this report is to offer information on the stormwater characteristics of the site in its existing and post construction condition.

For additional information regarding the site's existing conditions and the stormwater management system reference is made to the following plans and report;

Site Development Plans
 190 Washington St., Westwood, MA
 Owner: Skye Realty Management, LLC
 Prepared by; Marchionda & Assoc., L.P.

Dated; April 12, 2023

Existing Conditions:

The project site is located on the southeast side of the public way Washington Street in Westwood approximately 100 feet southwest of Wentworth Street. The property has a land area of 14,086 s.f. and is presently the site of a commercial office building with a bituminous concrete parking area. The property is presently accessed with two curb cuts onto Washington Street. The existing surface of the site is almost entirely made of impervious surfaces. The building, parking area and walkways amount to 12,100 s.f or 86% of the site.

The site abuts residential properties to north, south, and east. No areas of the site are located within a buffer zone to a wetland a resource area or a designated flood hazard area.

The majority of the stormwater from the existing site flows overland to a catch basin drywell in the existing parking area. A small portion of the property outside the perimeter of parking area flows either east to abutting properties or onto the Washington Street right of way and the municipal drainage system. Refer to the

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existing conditions plan in project site plans for specific information on the existing topography and features of the site.

Existing soils on the site have been recently explored by Marchionda & Associates. The observation holes revealed imported filled soils over gravelly loamy sands soils. Information on the site's soils has been included in appendix of the report.

Project Description:

The project consists of the renovation of the existing commercial use building and bituminous concrete parking lot. The development will include additions to the existing structure and will have a 2,285 s.f building footprint once completed. The parking area and drive aisles will be redesigned to provide a 13-car parking area and walkways to support the development.

The construction will require mostly shallow excavation and surface preparation and will be take place in areas that have been previously disturbed. Deeper excavations will be required in the areas of the proposed building additions and utilities. Based on the soil exploration preformed some exporting of unsuitable subsoils may be required.

When completed the development will have approximately 10,600 s.f. of impervious surfaces. This will result in a reduction of approximately 1.500 +/- s.f. of impervious surfaces. The remaining open space areas will be made up of manicured grass and landscape areas.

A comprehensive stormwater management system will be constructed to manage stormwater run-off generated by the project. This system will be made up a deep sump catch basin and an underground infiltration chamber system. All of the impervious surfaces on the property will drain to the new stormwater management system. Detailed information on the components of the system is included in the project's site plans.

Project Type:

The project will take place in areas previously disturbed. For purposes of stormwater management standards this project is considered a redevelopment project.

LID Measures:

When possible environmental sensitive site design and LID techniques have been used in the planning of the project. No construction will be required to take place within a wetland resource or buffer zone. All of the proposed construction will be located in areas previously disturbed by the existing facility.

Stormwater Management Standards Compliance:

A description of how this project meets the DEP stormwater standards, along with supporting documentation, is provided herein:

Standard 1: No New Untreated Stormwater Discharges

No new point source discharges will be created. The project has been designed to recharge a large portion of the storm water flows generated by the project.

Standard 2: No Increase in the Post-Development Peak Discharge Rate

Peak flow rates were studied under existing and proposed conditions for 2-year, 10-year, 25-year, and 100-year, 24-hour Type III storm events. Two study points (1 & 2) as shown in Figures 1 and 2 and as described below were developed to analyze runoff rates from the project site to the receiving wetland. The subcatchment watersheds to each study point were then delineated for the pre- and post-development conditions.

Study Point "1" represents the portion of the project that drains to the abutting properties to the east.

Study Point "2" represents the portion of the site that drains to the southwest to Washington Street and the municipal drainage system.

In terms of the modeling methodology, Technical Release 55 (TR-55) was utilized to obtain weighted curve numbers (CNs) for each of the pre- and post-development subcatchment areas. Inputs for obtaining the weighted CNs were based on ground cover type and hydrologic soil groups (HSGs). TR-55 was also utilized to obtain times of concentration (TCs) for each of the pre- and post-development subcatchment areas. Flow paths were generally broken into segments of sheet flow and shallow concentrated flow. Refer to attached TR-55 TC data (Appendix 1).

CNs and TCs obtained from TR-55 were input into the *Hydraflow*[®] Hydrographs software package, which utilizes the National Resources Conservation Service (NRCS) method to generate and route hydrographs.

As shown in the attached modeling output and as summarized in Table 1 (below), the peak runoff rate from the site in the proposed conditions for the design storms at the study points show an overall reduction in peak flows from the site.

TABLE 1: PEAK RUNOFF RATES FROM THE SITE AT EACH STUDY POINT

Study	2-yr storm event Study (3.24"/24-hr)		_	rm event /24-hr)	•	rm event /24-hr)	100-yr storm event (8.91"/24-hr)	
Point	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)	Pre (cfs)	Post (cfs)
1	1.0	0.0	1.5	0.0	1.9	0.1	2.2	0.8
2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1

Standard 3: Loss of Annual Recharge

DEP's Stormwater Management Handbook prescribes an infiltration volume based on the hydrologic soil group over which impervious area will be constructed as follows:

- HSG A 0.60 inches of runoff
- HSG B 0.35 inches of runoff
- HSG C 0.25 inches of runoff
- HSG D 0.10 inches of runoff

The proposed construction will include both the creation and removal of impervious surfaces. It appears from soil mapping and on-site soil observation that the entire project area is made up of soils that are considered to be in the hydrologic soil group "A".

A large portion of the stormwater run-off generated from the proposed impervious areas will be routed to the recharge system and will infiltrated into the soils within the project site. As a result, the proposed construction will meet and exceed the requirements for the loss of groundwater recharge.

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Standard 4: Water Quality

The project will maintain access drives and a parking area that will generate suspended solids. The project will however slightly reduce the area of paved surfaces from the present condition. By reducing the area of pavements the proposed development will reduce the amount of total suspended solids (TSS) generated. The project will also provide Stormwater Best Management Practices (BMP's) that will further reduce Total Suspended Solids generated for the site. The TSS removal BMP's proposed for the project include a hooded deep sump catch basin that will drain into an infiltration chambers system.

A Long-Term Stormwater Operation and Maintenance Plan & Pollution Prevention Plan (Appendix 4) has been developed for the project to comply with this requirement and the requirements of Standard 9.

Standard 5: Land Uses with Higher Potential Pollutant Loads

Not applicable – this project does not propose a land use with a higher potential pollutant load.

Standard 6: Discharges within a Zone II or Interim Wellhead Protection Area

The project site does not fall within a Zone II of a public water supply.

Standard 7: Redevelopment

This project is considered a redevelopment project as defined in the DEP *Stormwater Management Handbook*. As allowed, Standards 2, 3, & 4 are met to the extent practical.

Standard 8: Construction-Related Impacts

A Construction Period *Erosion & Sedimentation Control Plan* has been developed for the project. The project is not subject to the National Pollutant Discharge Elimination System (NPDES) program of the United States Environmental Protection Agency, as it will not involve greater than one acre of land disturbance.

April 12, 2023

Standard 9: Long-Term Operation and Maintenance

A Long-Term Stormwater Operation and Maintenance Plan & Pollution Prevention Plan has been developed for the project to comply with this requirement and the requirements of Standard 4. A copy of this plan has been included in the appendix of the report.

Standard 10: Illicit Discharges

DEP does not permit illicit discharges, defined by 310 CMR 10.04 as follows, to the stormwater management system:

"Illicit discharge means a discharge that is not entirely comprised of stormwater. Notwithstanding the foregoing, an illicit discharge does not include discharges from the following activities or facilities: firefighting, water line flushing, landscape irrigation, uncontaminated ground water, potable water sources, foundation drains, air conditioning condensation, footing drains, individual resident car washing, flows from riparian habitats and wetlands, dechlorinated water from swimming pools, water used for street washing and water used to clean buildings without detergents."

Prior to the discharge of stormwater runoff to the post-construction stormwater system it shall be the project owner's responsibility to prepare an Illicit Discharge Compliance Statement in accordance with Standard 10 certifying that no illicit discharges exist on the site.



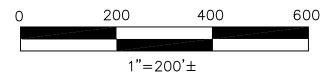


FIGURE 1: LOCUS MAP 190 WASHINGTON STREET

WESTWOOD, MASSACHUSETTS

SKYE REALTY MANAGEMENT, LLC 1208 VFW PARKWAY, SUITE 200

1208 VFW PARKWAY, SUITE 200 WEST ROXBURY, MA 02132

OCTOBER 2022 SCALE: 1"=400'±

Marchionda & Associates, L.P.

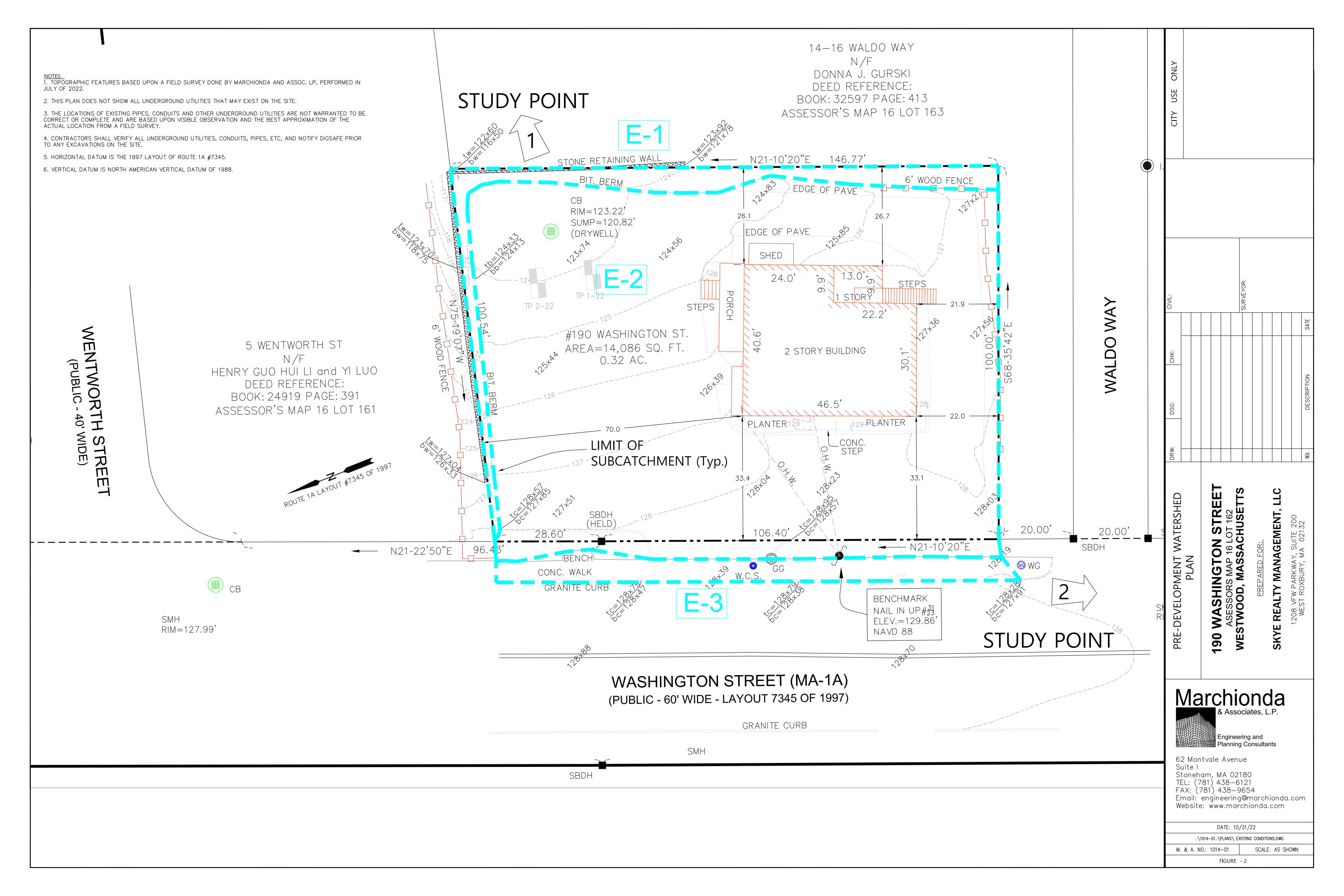
Engineering and Planning Consultants

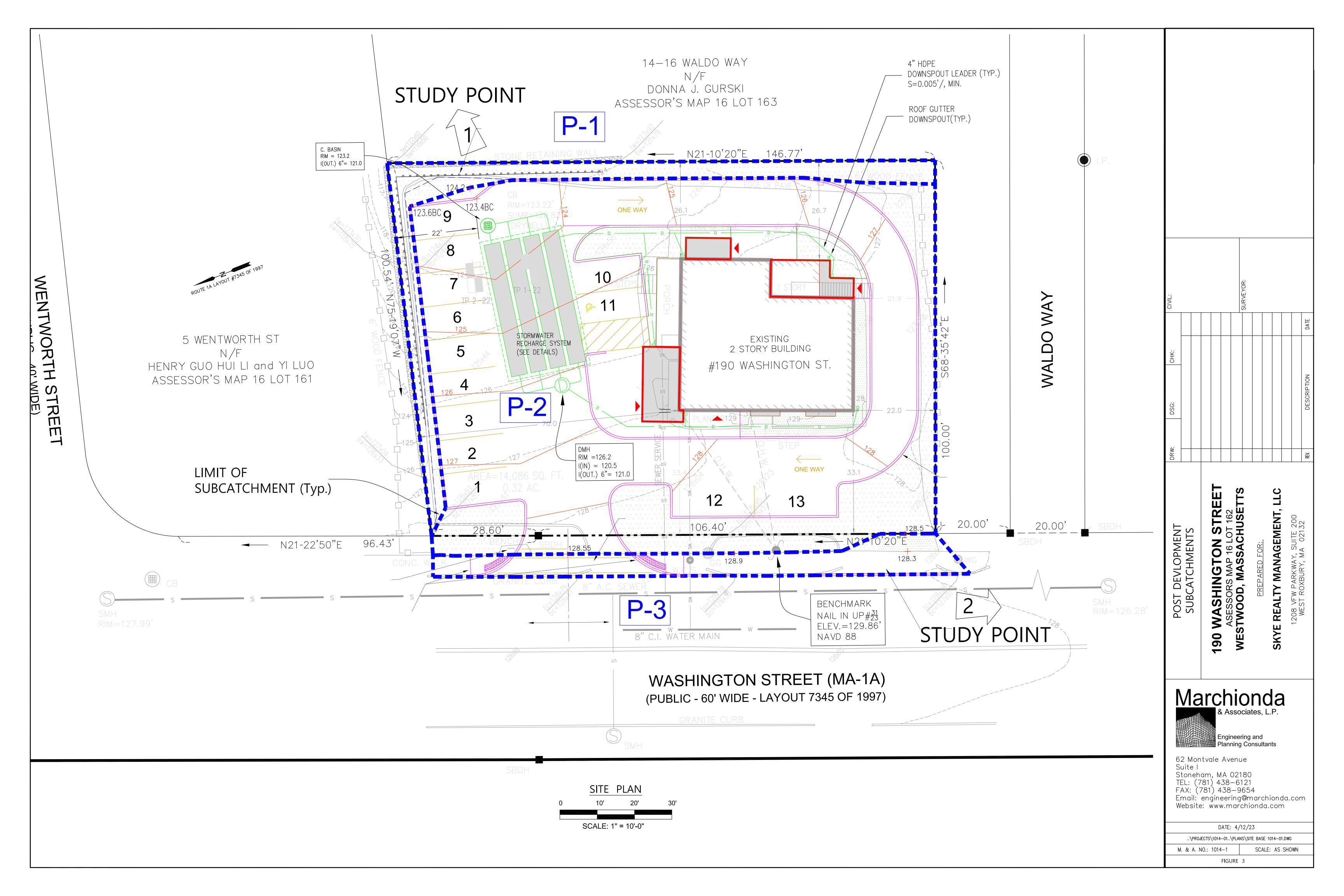
62 Montvale Avenue Suite I

TEL: (781) 438-6121 FAX: (781) 438-9654

Stoneham, MA 02180

Email: engineering@marchionda.com Website: www.marchionda.com





190 WASHINGTON STREET STORMWATER REPORT

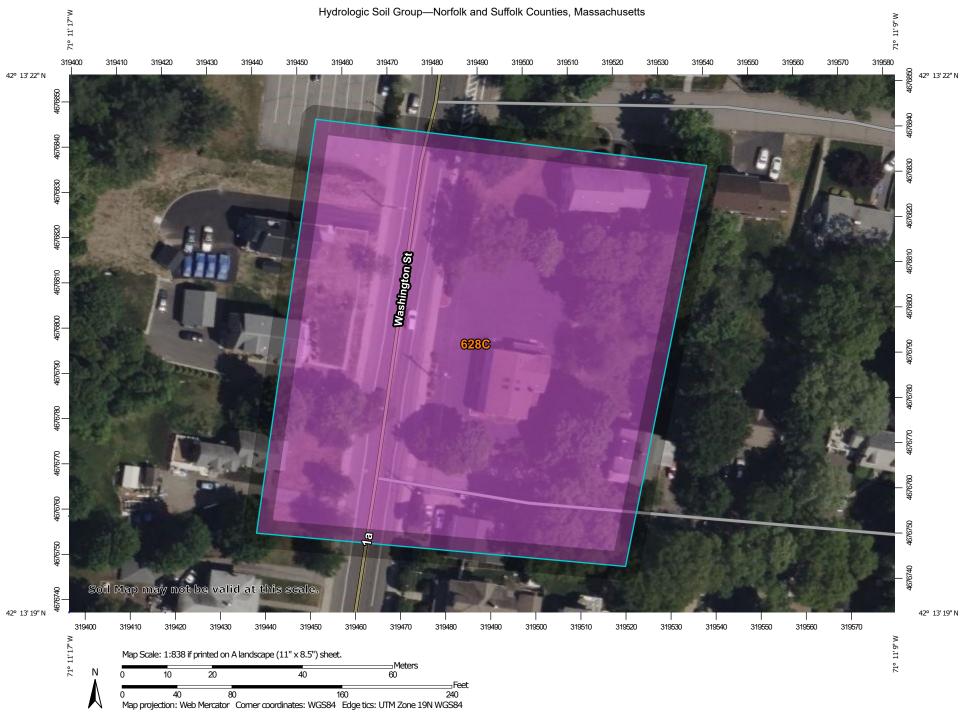
OCTOBER 31, 2022

LIST OF APPENDICES

Appendix 1	Standard 2 (Peak Flow)
Appendix 2	Standard 3 (Recharge)
Appendix 3	Standard 4 (TSS)
Appendix 4	Operation and Maintenance & Pollution Prevention Plan

APPENDIX 1 Standard 2 (Peak Flow)

SOILS INFORMATION



MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:25.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 18, Sep 9, 2022 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: May 22, 2022—Jun 5. 2022 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI					
628C	Canton-Urban land complex, 3 to 15 percent slopes	A	1.9	100.0%					
Totals for Area of Inter	est		1.9	100.0%					

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

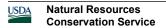
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Norfolk and Suffolk Counties, Massachusetts

628C—Canton-Urban land complex, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: vktb Elevation: 0 to 1,000 feet

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Canton and similar soils: 70 percent

Urban land: 20 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Canton

Setting

Landform: Ice-contact slopes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Friable coarse-loamy eolian deposits over loose

sandy and gravelly ablation till

Typical profile

H1 - 0 to 3 inches: fine sandy loam
H2 - 3 to 18 inches: fine sandy loam
H3 - 18 to 60 inches: gravelly loamy sand

Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 18 to 36 inches to strongly contrasting

textural stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High

(2.00 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Description of Urban Land

Setting

Parent material: Excavated and filled land

Minor Components

Montauk

Percent of map unit: 4 percent Hydric soil rating: No

Charlton

Percent of map unit: 2 percent Hydric soil rating: No

Scituate

Percent of map unit: 2 percent Hydric soil rating: No

Udorthents

Percent of map unit: 2 percent Hydric soil rating: Unranked

Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts

Survey Area Data: Version 18, Sep 9, 2022



Bureau of Resource Protection – Wastewater Permitting Program Form 11 - Soil Suitability Assessment Massachusetts Department of Environmental Protection

190 WASHINGTON ST.

Site Address or Map/Lot Number

Westwood

Deep Observation Hole

Deep Hole Number:

								N		
Other								12/21/2		
Soil Consistence (Moist)				入爪	シガ	> T.		1. J. BAPROWS MASE #84 DATE: 12/21/22	280"	
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DEP Form 11 Soil Suitability Assessment



Massachusetts Department of Environmental Protection Bureau of Resource Protection – Wastewater Permitting Program Form 11 - Soil Suitability Assessment

MOWASHINGTON ST.
Site Address or Map/Lot Number

WASTAWOOD

Deep Observation Hole

Deep Hole Number: 2-22

								24
Other								2 2
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Soil Horizon/ Laver	,)	4	B	U		Additional Notes
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CURVE NUMBER COMPUTATIONS

Project 190 WASHINGTON ST. By JB Date 10/31/22							31/22	
Location VESTV		Checked				Date		
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Soil name	Cover description			CN ¹		Area	Product of	
and hydrologic							CN x area	
group	(cover type, treatment, and hydrologic of	ondition, percent	Table 2-2	igure 2-3	Figure 2-4	© acres □ mi ²		
(appendix A)	impervious, unconnected/connected imp	ervious area ratio)	Tab	Figu	Figi	□%		
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		74199						
1/								
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Runoff, Q	in	8				\top		
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2. Runoff				
		Storm #1	Storm #2	Storm #3
Frequency	yryr			
Rainfall, P	(24-hour) in			
	in		6-18-	
	d CN with table 2-1, figure 2-1, or 2-3 and 2-4)			

Project 190 WASHINGTON ST. By JiB,							Date 10-3/-22		
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			Storm #1		Storn	n #2		Storm #3	
Frequency		yr							
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Project 190 WASHINGTON ST.					By				Date 11/17/22	
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Project 190 WA	SHINGTON ST.	By 78)	.	Date 11/17/22		
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and hydrologic						CN x area	
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(appendix A)	impervious unconnected/connected imper	vious area ratio)	Tabl Figure	Ē, C	□%		
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Project 190 WA	ASHINGTON ST.	By JE		Date /17/22
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	ent Developed 11 P	3"		
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Soil name and hydrologic group	Cover description	condition; percent	Table 2-2 Figure 2-3 Figure 2-4	Area Product of CN x area
(appendix A)	impervious; unconnected/connected in		Pig. Fig.	0.02
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Rainfall, F	(24-hour) in			
I .	in			
	nd CN with table 2-1, figure 2-1, or 2-3 and 2-4)		36 P	

HYDROGRAPHS

Hydrograph Return Period Recap

Hydraflow Hydrographs by Intelisolve v9.2

Hyd. No.	Hydrograph type (origin)	Inflow Hyd(s)				Hydrograph					
			1-Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	description
1	SCS Runoff			0.000			0.000	0.003		0.006	E-1
2	SCS Runoff			0.911			1.420	1.812		2.089	E-2
3	SCS Runoff			0.062			0.093	0.117		0.134	E-3
4	Reservoir	2		0.908			1.414	1.805		2.081	Ex. DW outflow
5	Combine	2, 3,		0.973			1.513	1.929		2.223	Flow to SP #1 (Pre)
6	SCS Runoff			0.000			0.000	0.003		0.006	P-1
7	SCS Runoff			0.537			1.024	1.418		1.701	P-2
8	SCS Runoff			0.062			0.093	0.117		0.134	P-3
9	Reservoir	7		0.000			0.000	0.126		0.829	RA #1 Outflow
10	Combine	6, 9		0.000			0.000	0.127		0.835	Flow to SP #1 (Post)

Proj. file: HYDRO.gpw

Thursday, Apr 6, 2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description	
1	SCS Runoff	0.000	1	n/a	0				E-1	
2	SCS Runoff	0.911	1	724	2,931				E-2	
3	SCS Runoff	0.062	1	724	215				E-3	
4	Reservoir	0.908	1	724	2,636	2	123.75	195	Ex. DW outflow	
5	Combine	0.973	1	724	3,146	2, 3,			Flow to SP #1 (Pre)	
6	SCS Runoff	0.000	1	n/a	0				P-1	
7	SCS Runoff	0.537	1	725	1,666				P-2	
8	SCS Runoff	0.062	1	724	215				P-3	
9	Reservoir	0.000	1	704	0	7	119.87	738	RA #1 Outflow	
10	Combine	0.000	1	704	0	6, 9			Flow to SP #1 (Post)	
HYDRO.gpw					Return P	eriod: 2 Ye	ar	Thursday, Apr 6, 2023		

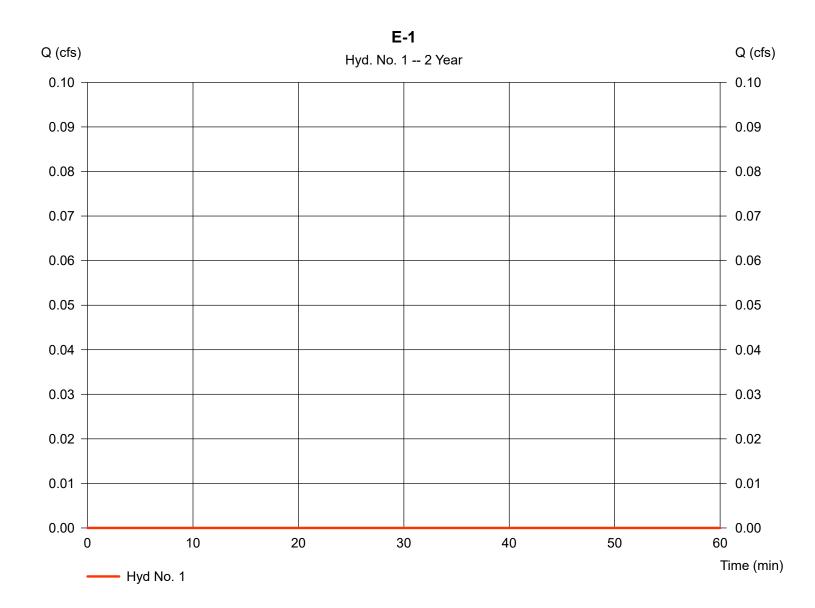
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 1

E-1

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency Time to peak = 2 yrs = n/aTime interval = 1 min Hyd. volume = 0 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 3.10 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

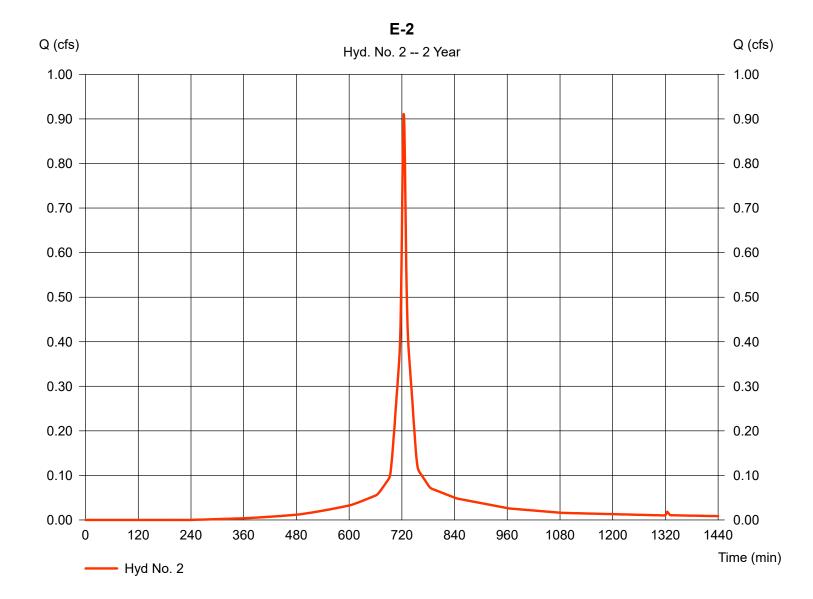
Thursday, Apr 6, 2023

Hyd. No. 2

E-2

Hydrograph type = SCS Runoff Storm frequency = 2 yrsTime interval = 1 min Drainage area = 0.320 acBasin Slope = 0.0 % Tc method = USER Total precip. = 3.10 inStorm duration = 24 hrs

Peak discharge = 0.911 cfs= 724 min Time to peak Hyd. volume = 2,931 cuftCurve number = 94 Hydraulic length = 0 ftTime of conc. (Tc) $= 6.00 \, \text{min}$ Distribution = Type III = 484 Shape factor



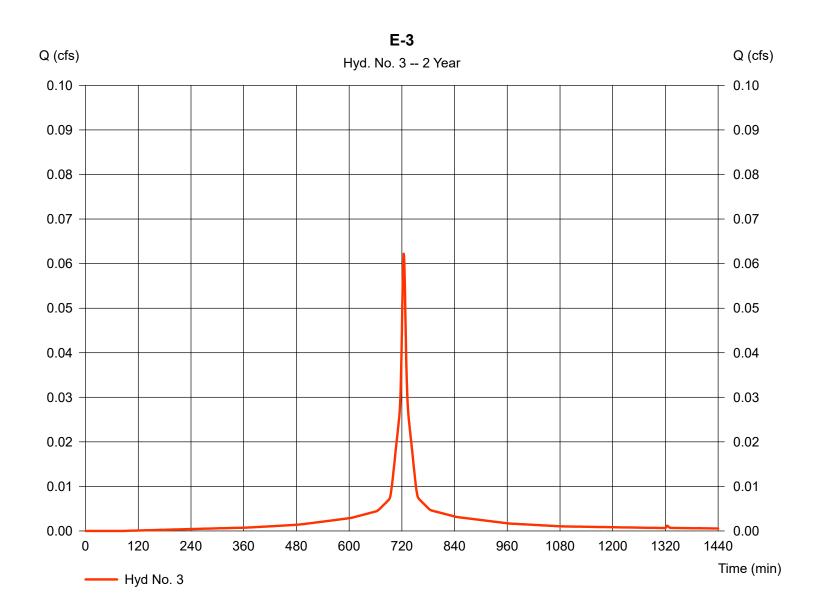
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 3

E-3

Hydrograph type = SCS Runoff Peak discharge = 0.062 cfsStorm frequency Time to peak = 724 min = 2 yrsTime interval = 1 min Hyd. volume = 215 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 3.10 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

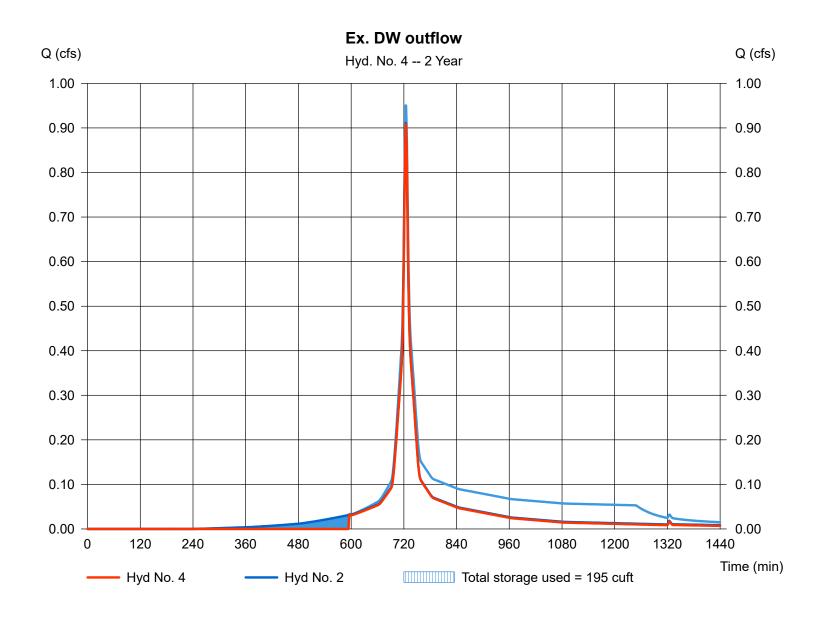
Thursday, Apr 6, 2023

Hyd. No. 4

Ex. DW outflow

Hydrograph type = Reservoir Peak discharge = 0.908 cfsStorm frequency Time to peak = 2 yrs = 724 min Time interval = 1 min Hyd. volume = 2,636 cuftInflow hyd. No. = 2 - E - 2Max. Elevation = 123.75 ft= Ex. Drywell Reservoir name Max. Storage = 195 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Pond No. 1 - Ex. Drywell

Pond Data

UG Chambers - Invert elev. = 120.80 ft, Rise x Span = 2.40 x 3.50 ft, Barrel Len = 4.00 ft, No. Barrels = 1, Slope = 0.00%, Headers = No **Encasement** - Invert elev. = 119.80 ft, Width = 7.50 ft, Height = 3.40 ft, Voids = 40.00%

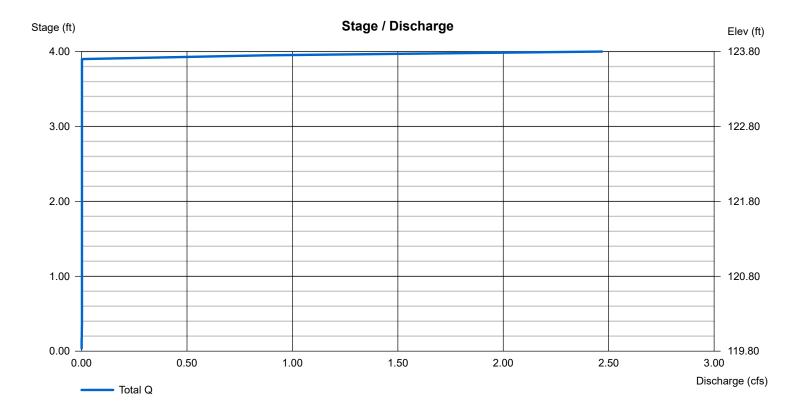
Contours - User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 123.30 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	119.80	n/a	0	0
0.34	120.14	n/a	4	4
0.68	120.48	n/a	4	8
1.02	120.82	n/a	4	12
1.36	121.16	n/a	7	19
1.70	121.50	n/a	7	26
2.04	121.84	n/a	7	33
2.38	122.18	n/a	7	40
2.72	122.52	n/a	7	47
3.06	122.86	n/a	7	54
3.40	123.20	n/a	7	61
3.50	123.30	50	2	63
4.00	123.80	650	147	209

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] = 0.000.00 0.00 0.00 = 30.00 0.00 0.00 0.00 Rise (in) Crest Len (ft) = 0.000.00 0.00 0.00 Crest El. (ft) = 123.700.00 0.00 0.00 Span (in) = 00 0 Weir Coeff. = 260No. Barrels 0 3.33 3.33 3.33 Invert El. (ft) = 0.000.00 0.00 0.00 **Weir Type** = Broad Length (ft) = 0.000.00 0.00 0.00 Multi-Stage = No No No No = 0.000.00 0.00 Slope (%) n/a = .013 .013 .013 N-Value n/a = 0.600.60 0.60 0.60 = 2.410 (by Contour) Orifice Coeff. Exfil.(in/hr) Multi-Stage = n/aNo No TW Elev. (ft) = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



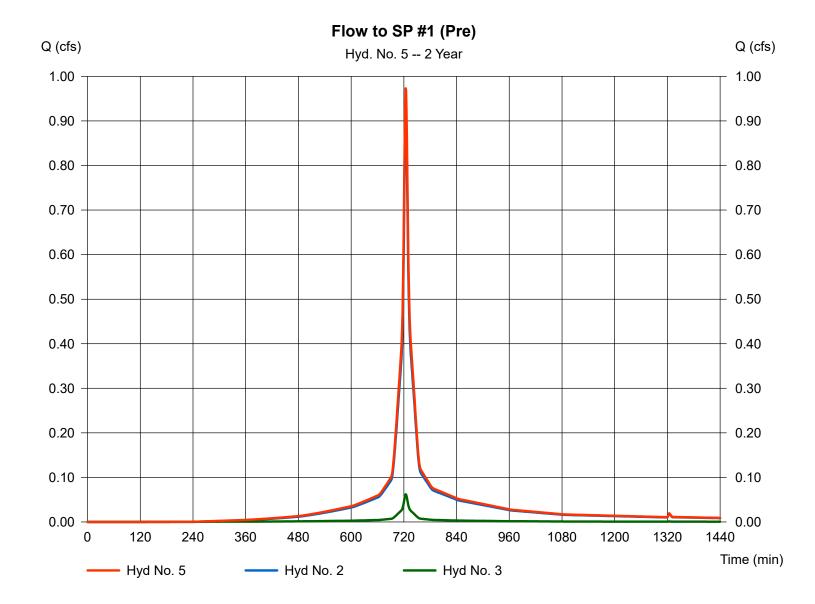
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 5

Flow to SP #1 (Pre)

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 2, 3 Peak discharge = 0.973 cfs
Time to peak = 724 min
Hyd. volume = 3,146 cuft
Contrib. drain. area = 0.340 ac



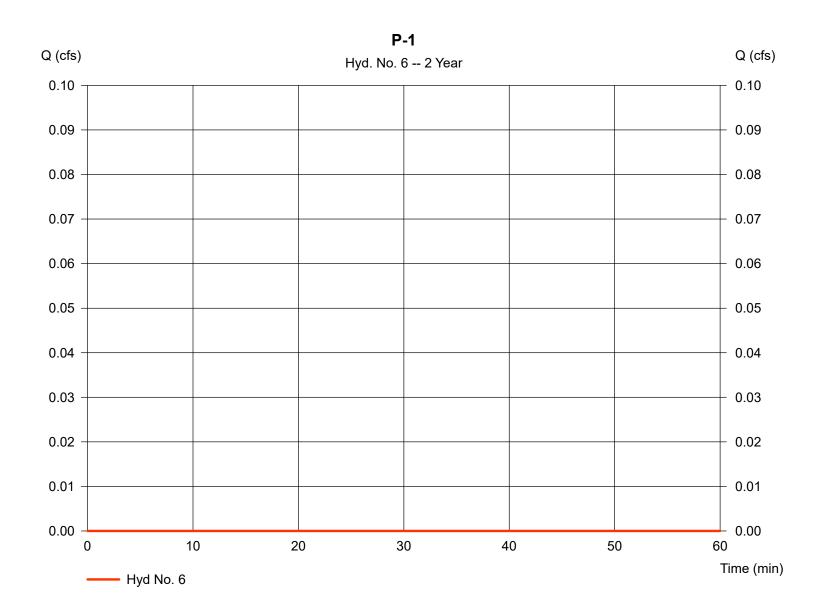
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 6

P-1

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency Time to peak = 2 yrs = n/aTime interval = 1 min Hyd. volume = 0 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 3.10 in= Type III Storm duration = 484 = 24 hrs Shape factor



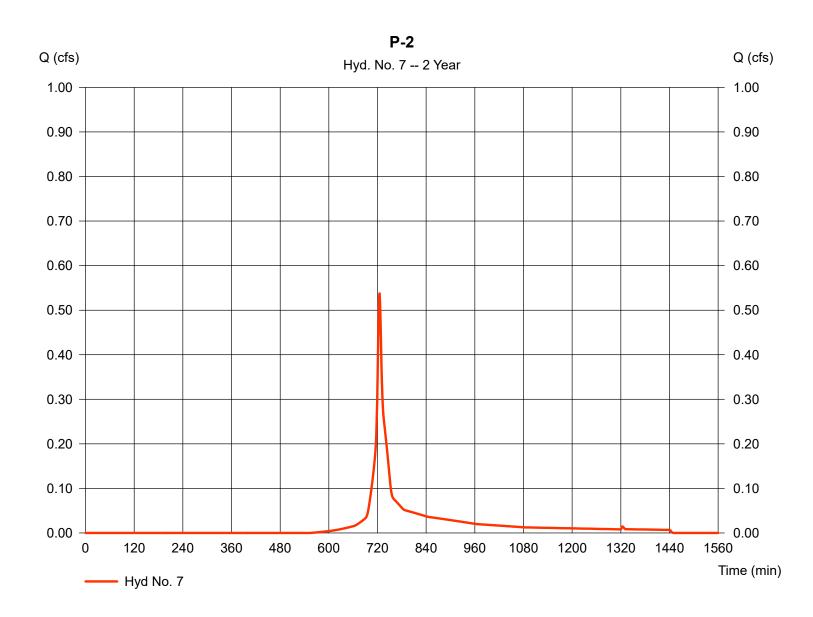
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 7

P-2

Hydrograph type = SCS Runoff Peak discharge = 0.537 cfsStorm frequency Time to peak = 2 yrs= 725 min Time interval = 1 min Hyd. volume = 1,666 cuft Drainage area = 0.320 acCurve number = 81 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 3.10 in= Type III Storm duration = 484 = 24 hrs Shape factor



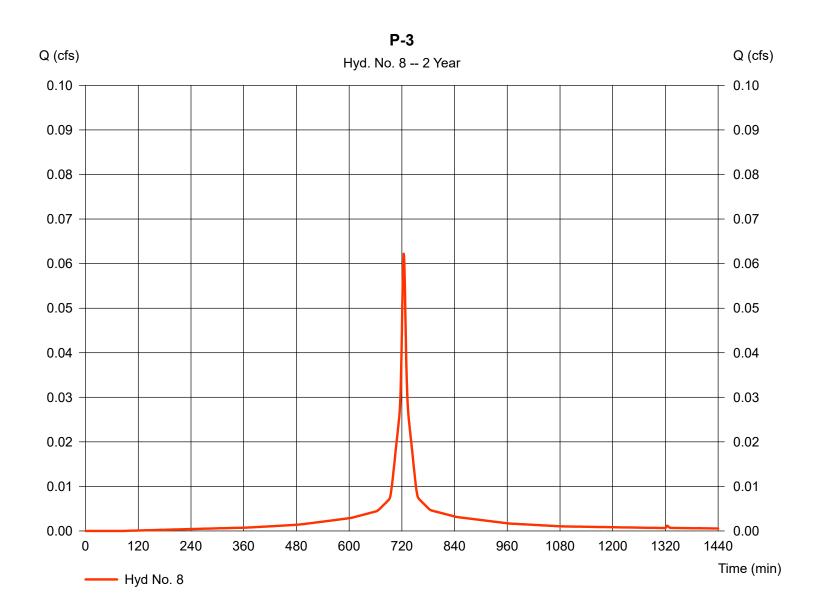
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 8

P-3

Hydrograph type = SCS Runoff Peak discharge = 0.062 cfsStorm frequency Time to peak = 724 min = 2 yrs= 1 min Time interval Hyd. volume = 215 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 3.10 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

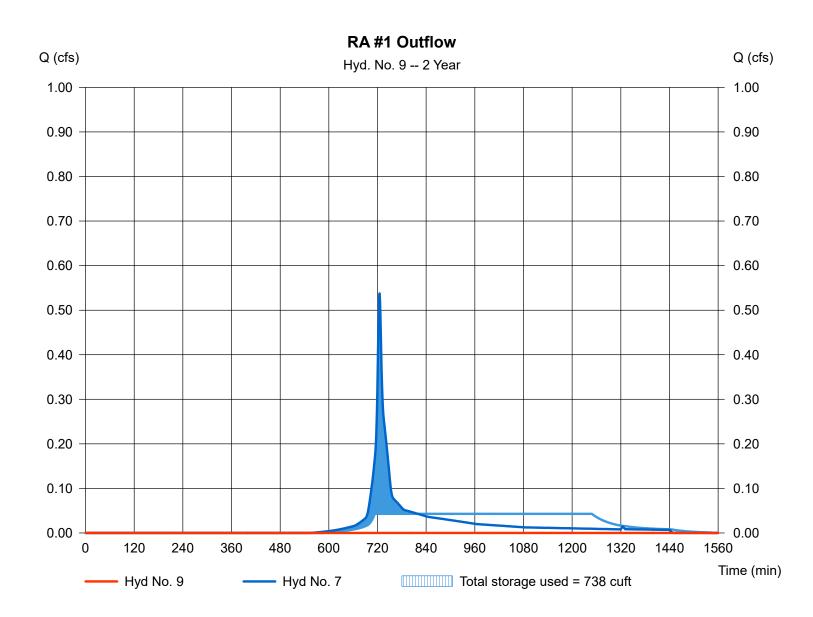
Thursday, Apr 6, 2023

Hyd. No. 9

RA#1 Outflow

Hydrograph type = Reservoir Peak discharge = 0.000 cfsStorm frequency Time to peak = 2 yrs = 704 min Time interval = 1 min Hyd. volume = 0 cuft Inflow hyd. No. = 7 - P-2Max. Elevation = 119.87 ftReservoir name = RA #1 Max. Storage = 738 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



Pond No. 2 - RA #1

Pond Data

UG Chambers - Invert elev. = 119.00 ft, Rise x Span = 2.50 x 4.33 ft, Barrel Len = 36.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = No **Encasement** - Invert elev. = 118.50 ft, Width = 5.33 ft, Height = 4.00 ft, Voids = 40.00%

Contours - User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 122.60 ft

Stage / Storage Table

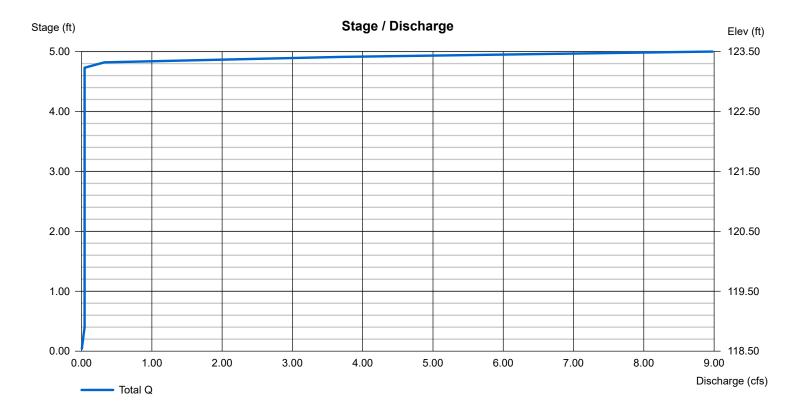
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	118.50	n/a	0	0
0.40	118.90	n/a	123	123
0.80	119.30	n/a	235	358
1.20	119.70	n/a	269	627
1.60	120.10	n/a	262	889
2.00	120.50	n/a	250	1,140
2.40	120.90	n/a	232	1,372
2.80	121.30	n/a	203	1,575
3.20	121.70	n/a	143	1,717
3.60	122.10	n/a	123	1,840
4.00	122.50	n/a	123	1,963
4.10	122.60	50	2	1,965
5.00	123.50	800	315	2,280

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 30.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 123.30	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.410 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



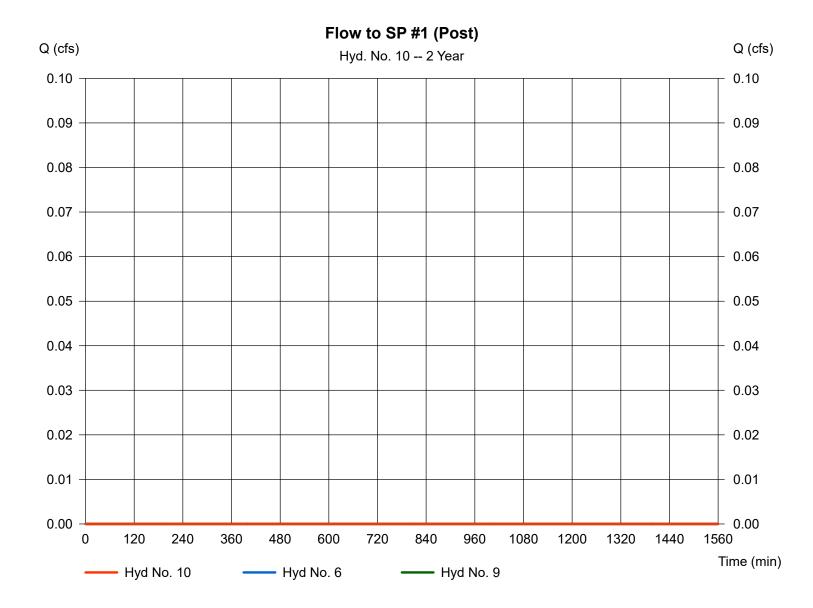
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 10

Flow to SP #1 (Post)

Hydrograph type = Combine Storm frequency = 2 yrs Time interval = 1 min Inflow hyds. = 6, 9 Peak discharge = 0.000 cfs
Time to peak = 704 min
Hyd. volume = 0 cuft
Contrib. drain. area = 0.020 ac



2 SCS Runoff 1.420 1 724 4,688 E-2 3 SCS Runoff 0.093 1 724 327 E-3 4 Reservoir 1.414 1 725 4,385 2 123.77 200 Ex. DW outflow 5 Combine 1.513 1 724 5,015 2, 3, Flow to SP #1 (Pre) 6 SCS Runoff 0.000 1 874 9 P-1 7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA #1 Outflow	Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
3 SCS Runoff 0.093 1 724 327 E-3 4 Reservoir 1.414 1 725 4,385 2 123.77 200 Ex. DW outflow 5 Combine 1.513 1 724 5,015 2, 3, Flow to SP #1 (Pre) 6 SCS Runoff 0.000 1 874 9 P-1 7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA#1 Outflow	1	SCS Runoff	0.000	1	874	9				E-1
4 Reservoir 1.414 1 725 4,385 2 123.77 200 Ex. DW outflow 5 Combine 1.513 1 724 5,015 2, 3, Flow to SP #1 (Pre) 6 SCS Runoff 0.000 1 874 9 P-1 7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA#1 Outflow	2	SCS Runoff	1.420	1	724	4,688				E-2
5 Combine 1.513 1 724 5,015 2, 3, Flow to SP #1 (Pre) 6 SCS Runoff 0.000 1 874 9 P-1 7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA #1 Outflow	3	SCS Runoff	0.093	1	724	327				E-3
6 SCS Runoff 0.000 1 874 9 P-1 7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA#1 Outflow	4	Reservoir	1.414	1	725	4,385	2	123.77	200	Ex. DW outflow
7 SCS Runoff 1.024 1 725 3,156 P-2 8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA#1 Outflow	5	Combine	1.513	1	724	5,015	2, 3,			Flow to SP #1 (Pre)
8 SCS Runoff 0.093 1 724 327 P-3 9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA#1 Outflow	6	SCS Runoff	0.000	1	874	9				P-1
9 Reservoir 0.000 1 665 0 7 121.86 1,767 RA #1 Outflow	7	SCS Runoff	1.024	1	725	3,156				P-2
	8	SCS Runoff	0.093	1	724	327				P-3
10 Combine 0.000 1 874 9 6.9 Flow to SP#1 (Post)	9	Reservoir	0.000	1	665	0	7	121.86	1,767	RA #1 Outflow
	10	Combine	0.000	1	874	9	6, 9			Flow to SP #1 (Post)

Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

= 0.000 cfs

= 874 min

 $= 6.00 \, \text{min}$

= Type III

= 9 cuft

= 39

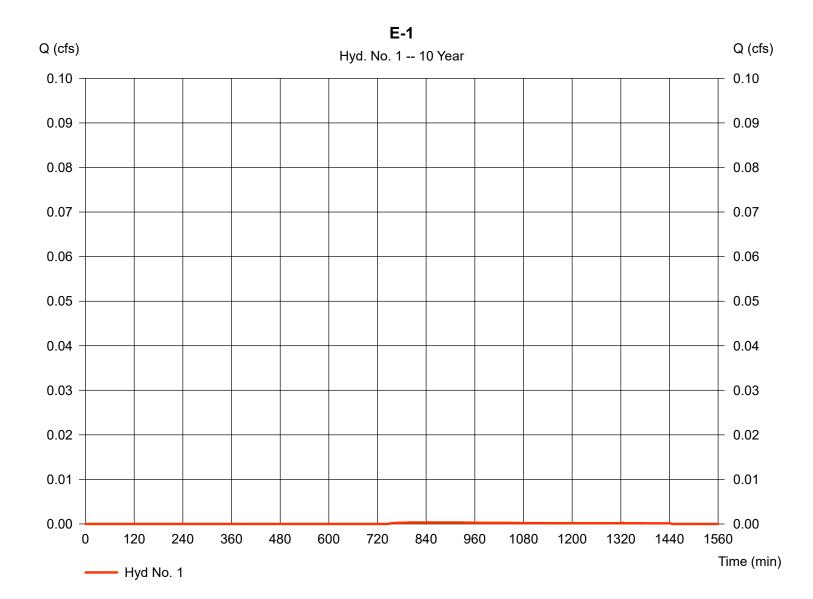
= 0 ft

= 484

Hyd. No. 1

E-1

= SCS Runoff Hydrograph type Peak discharge Storm frequency Time to peak = 10 yrsTime interval = 1 min Hyd. volume Drainage area = 0.020 acCurve number Basin Slope = 0.0 % Hydraulic length Tc method = USER Time of conc. (Tc) Distribution Total precip. = 4.60 inStorm duration = 24 hrs Shape factor



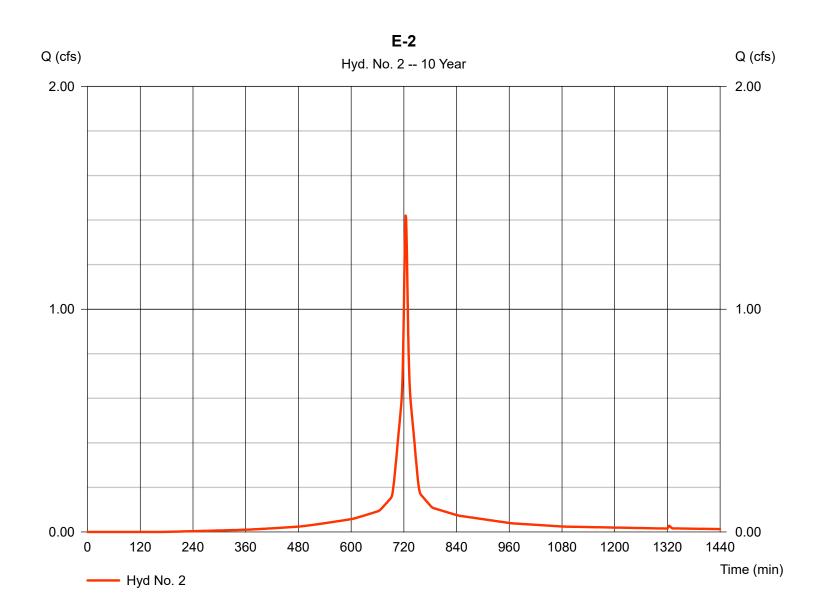
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 2

E-2

Hydrograph type = SCS Runoff = 1.420 cfsPeak discharge Storm frequency Time to peak = 724 min = 10 yrsTime interval = 1 min Hyd. volume = 4,688 cuft Drainage area = 0.320 acCurve number = 94 Basin Slope = 0.0 % Hydraulic length = 0 ftTime of conc. (Tc) Tc method = USER $= 6.00 \, \text{min}$ Distribution Total precip. = 4.60 in= Type III Storm duration = 24 hrs = 484 Shape factor



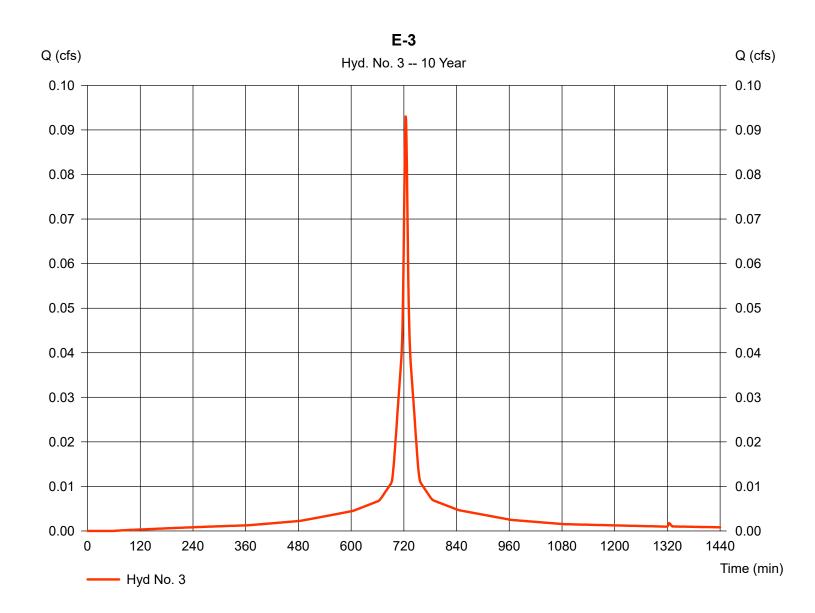
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 3

E-3

Hydrograph type = SCS Runoff Peak discharge = 0.093 cfsStorm frequency Time to peak = 10 yrs= 724 min Time interval = 1 min Hyd. volume = 327 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 4.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

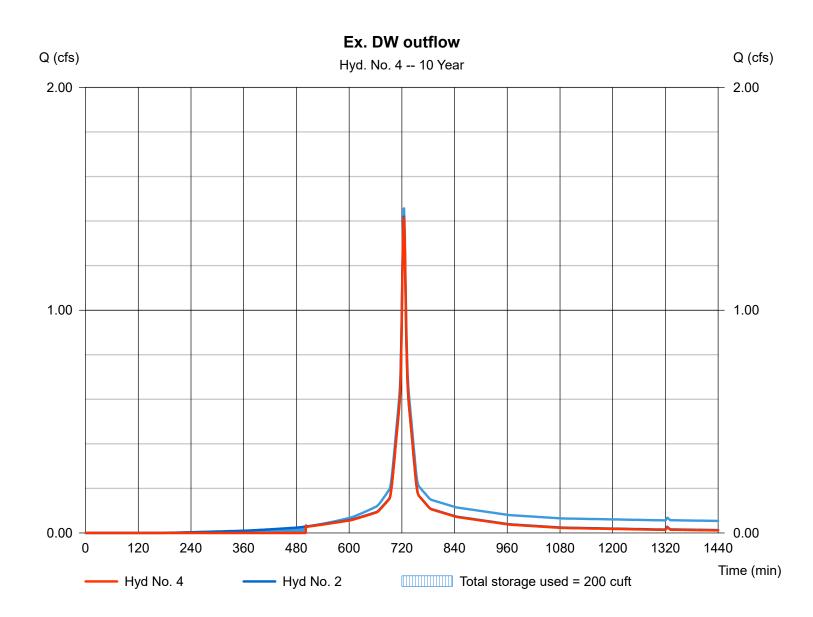
Thursday, Apr 6, 2023

Hyd. No. 4

Ex. DW outflow

Hydrograph type = Reservoir Peak discharge = 1.414 cfsStorm frequency Time to peak = 725 min = 10 yrsTime interval = 1 min Hyd. volume = 4,385 cuftInflow hyd. No. = 2 - E - 2Max. Elevation = 123.77 ftReservoir name = Ex. Drywell Max. Storage = 200 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



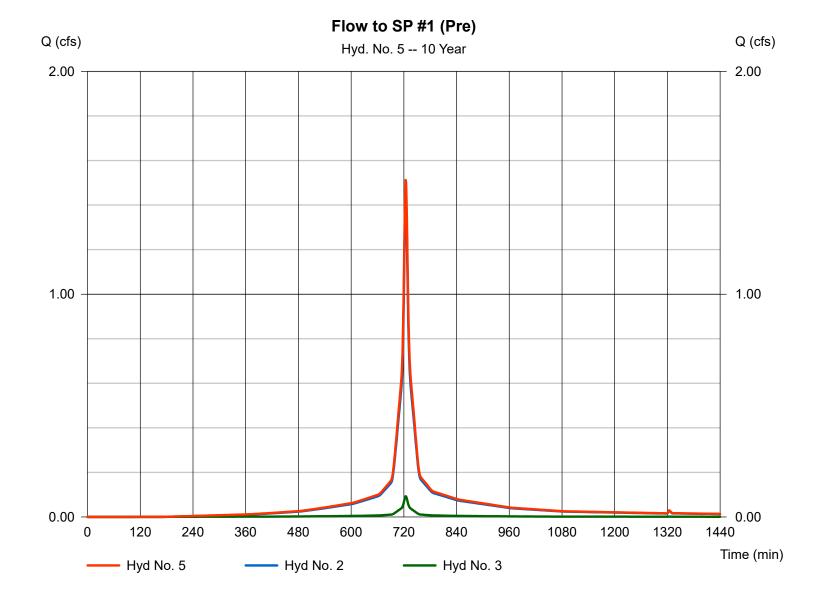
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 5

Flow to SP #1 (Pre)

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 2, 3 Peak discharge = 1.513 cfs
Time to peak = 724 min
Hyd. volume = 5,015 cuft
Contrib. drain. area = 0.340 ac



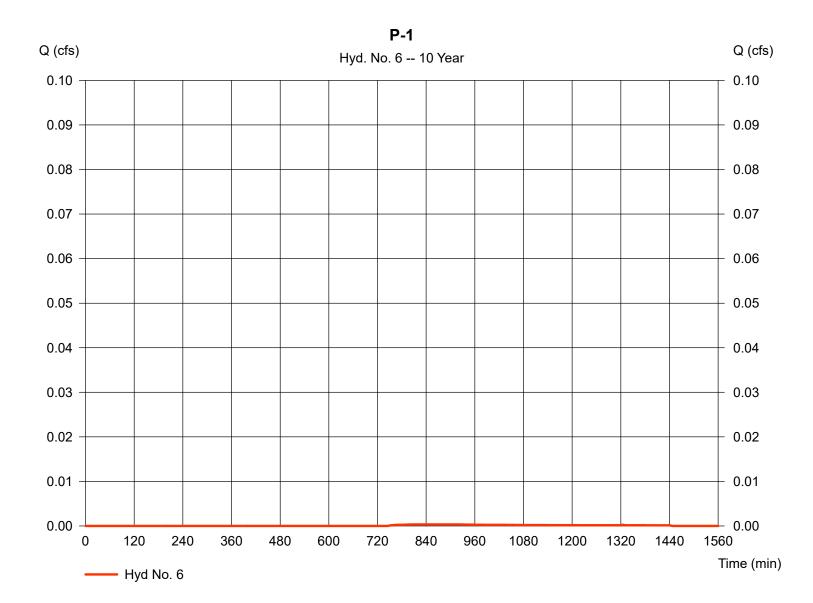
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 6

P-1

Hydrograph type = SCS Runoff Peak discharge = 0.000 cfsStorm frequency Time to peak = 10 yrs= 874 min Time interval = 1 min Hyd. volume = 9 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 4.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



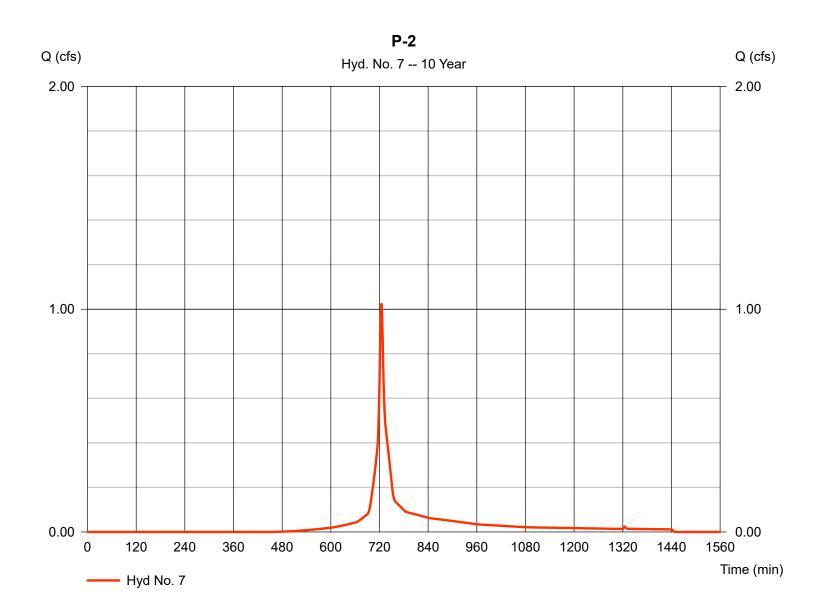
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 7

P-2

Hydrograph type = SCS Runoff = 1.024 cfsPeak discharge Storm frequency Time to peak = 725 min = 10 yrs Time interval = 1 min Hyd. volume = 3,156 cuftDrainage area = 0.320 acCurve number = 81 Basin Slope = 0.0 % Hydraulic length = 0 ftTime of conc. (Tc) Tc method = USER $= 6.00 \, \text{min}$ Distribution Total precip. = 4.60 in= Type III Storm duration = 24 hrs = 484 Shape factor



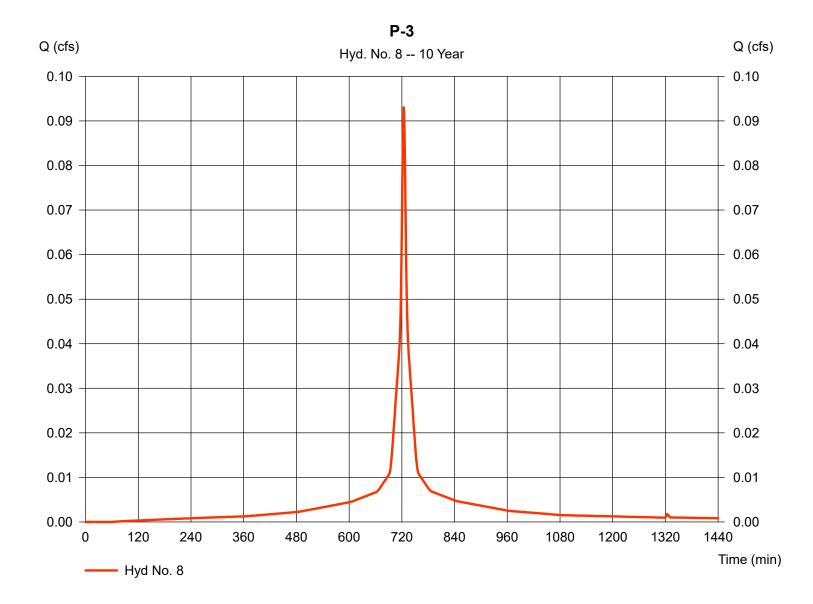
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 8

P-3

Hydrograph type = SCS Runoff Peak discharge = 0.093 cfsStorm frequency Time to peak = 10 yrs= 724 min Time interval = 1 min Hyd. volume = 327 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 4.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

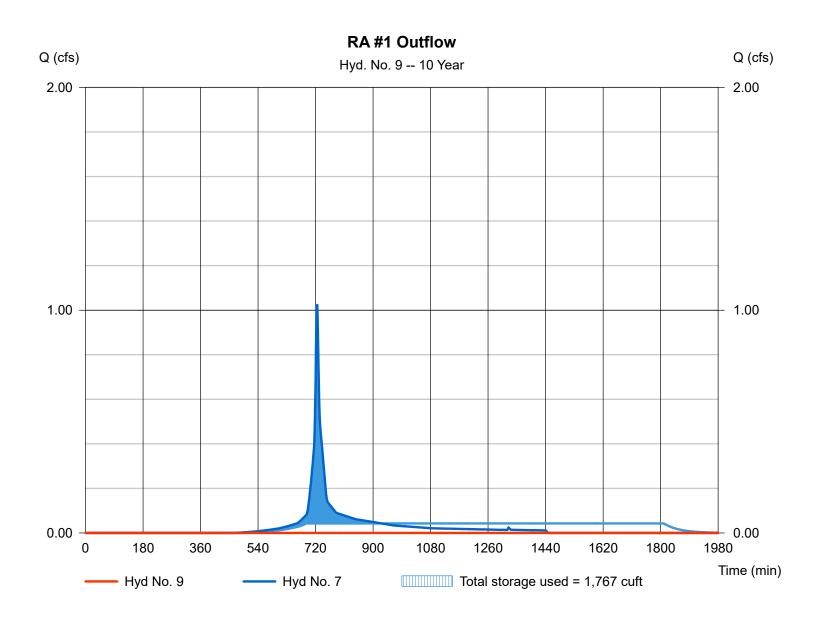
Thursday, Apr 6, 2023

Hyd. No. 9

RA#1 Outflow

Hydrograph type = Reservoir Peak discharge = 0.000 cfsStorm frequency Time to peak = 10 yrs= 665 min Time interval = 1 min Hyd. volume = 0 cuft Inflow hyd. No. = 7 - P-2Max. Elevation = 121.86 ftReservoir name = RA #1Max. Storage = 1,767 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



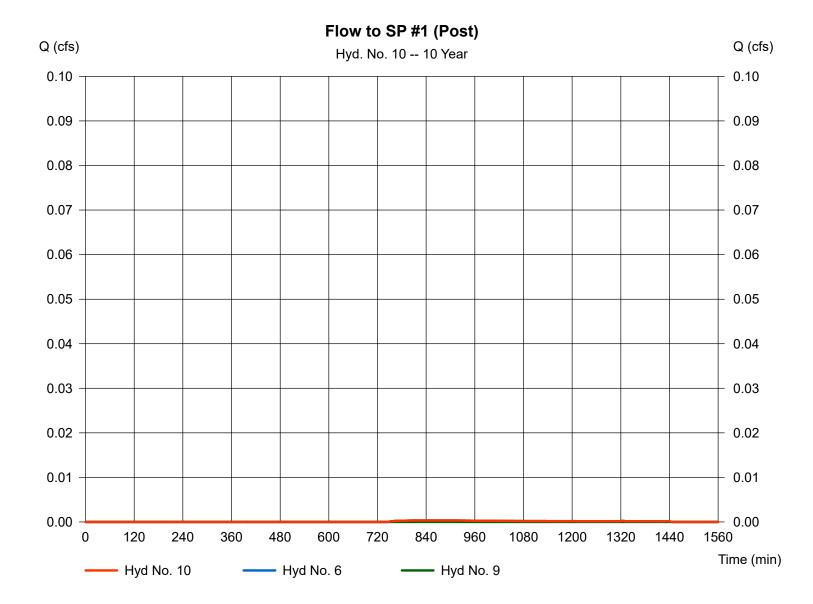
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 10

Flow to SP #1 (Post)

Hydrograph type = Combine Storm frequency = 10 yrs Time interval = 1 min Inflow hyds. = 6, 9 Peak discharge = 0.000 cfs
Time to peak = 874 min
Hyd. volume = 9 cuft
Contrib. drain. area = 0.020 ac



		Hydrallow Hydrographs by Intell						, a. a	
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.003	1	741	29				E-1
2	SCS Runoff	1.812	1	724	6,072				E-2
3	SCS Runoff	0.117	1	724	414				E-3
4	Reservoir	1.805	1	724	5,764	2	123.78	203	Ex. DW outflow
5	Combine	1.929	1	724	6,486	2, 3,			Flow to SP #1 (Pre)
6	SCS Runoff	0.003	1	741	29				P-1
7	SCS Runoff	1.418	1	725	4,402				P-2
3	SCS Runoff	0.117	1	724	414				P-3
9	Reservoir	0.126	1	765	531	7	123.27	2,199	RA #1 Outflow
10	Combine	0.127	1	765	559	6, 9			Flow to SP #1 (Post)
HYI	DRO.gpw				Return F	Period: 25 Y	 ′ear	Thursday, A	 Apr 6, 2023

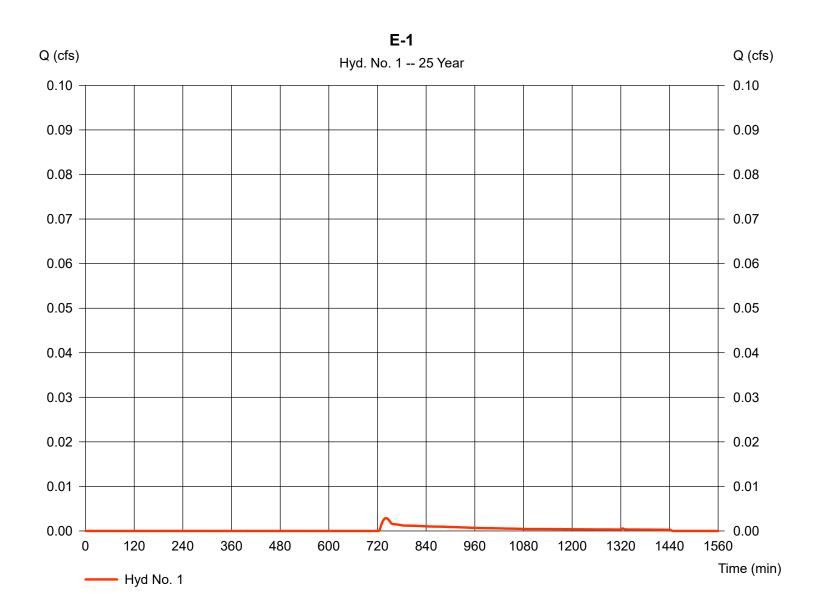
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 1

E-1

Hydrograph type = SCS Runoff Peak discharge = 0.003 cfsStorm frequency Time to peak = 741 min = 25 yrs Time interval = 1 min Hyd. volume = 29 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 5.77 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

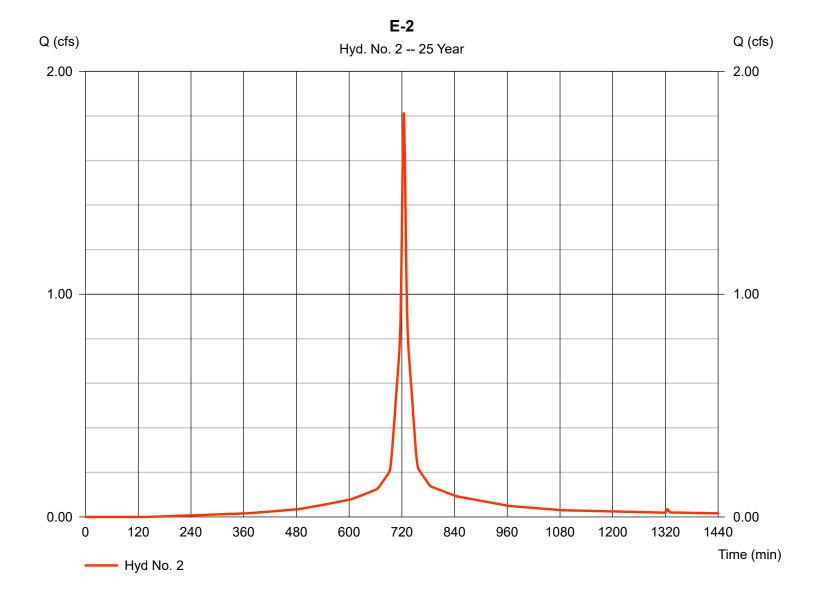
Thursday, Apr 6, 2023

Hyd. No. 2

E-2

Hydrograph type = SCS Runoff Storm frequency = 25 yrs Time interval = 1 min Drainage area = 0.320 acBasin Slope = 0.0 % Tc method = USER Total precip. = 5.77 inStorm duration = 24 hrs

Peak discharge = 1.812 cfsTime to peak = 724 min Hyd. volume = 6,072 cuftCurve number = 94 Hydraulic length = 0 ftTime of conc. (Tc) $= 6.00 \, \text{min}$ Distribution = Type III = 484 Shape factor



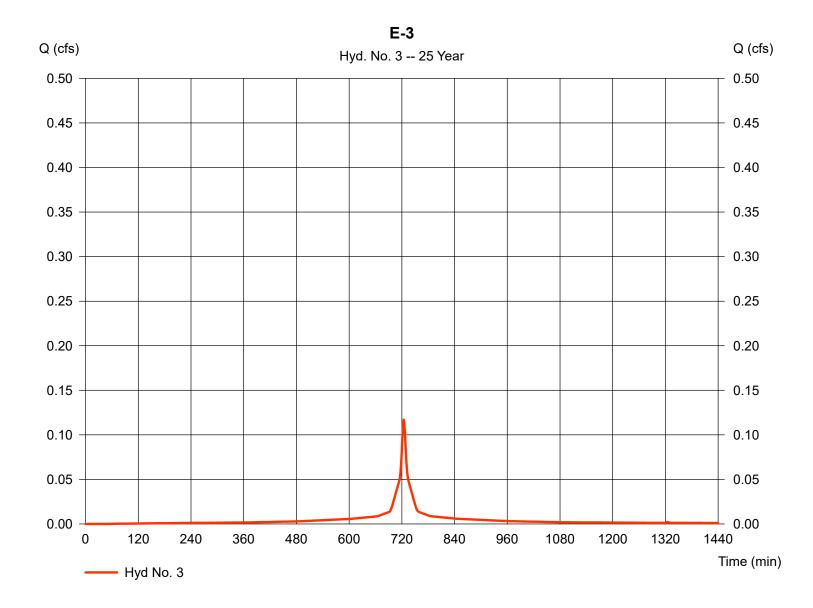
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 3

E-3

Hydrograph type = SCS Runoff = 0.117 cfsPeak discharge Storm frequency Time to peak = 724 min = 25 yrs Time interval = 1 min Hyd. volume = 414 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 5.77 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

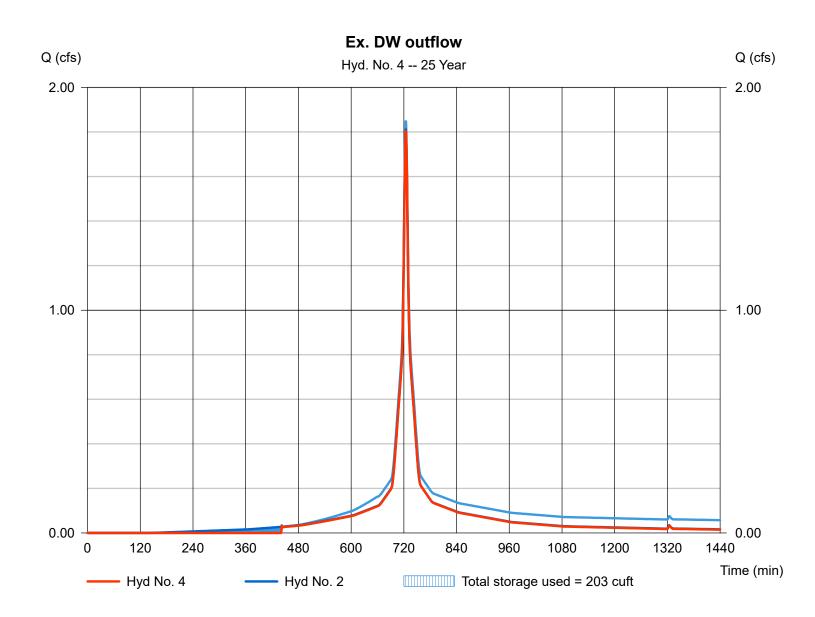
Thursday, Apr 6, 2023

Hyd. No. 4

Ex. DW outflow

Hydrograph type = 1.805 cfs= Reservoir Peak discharge Storm frequency Time to peak = 724 min = 25 yrs Time interval = 1 min Hyd. volume = 5,764 cuftInflow hyd. No. = 2 - E - 2Max. Elevation = 123.78 ftReservoir name = Ex. Drywell Max. Storage = 203 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



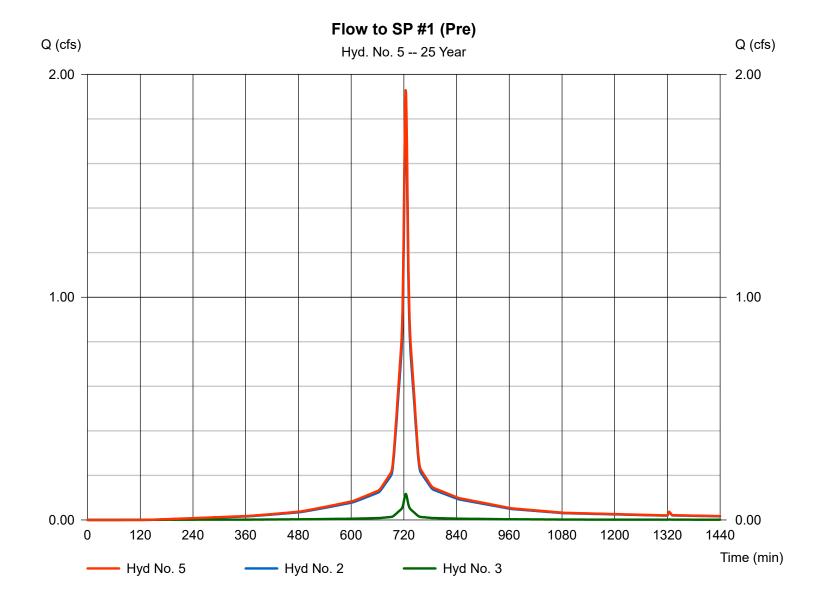
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 5

Flow to SP #1 (Pre)

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 1 min Inflow hyds. = 2, 3 Peak discharge = 1.929 cfs
Time to peak = 724 min
Hyd. volume = 6,486 cuft
Contrib. drain. area = 0.340 ac



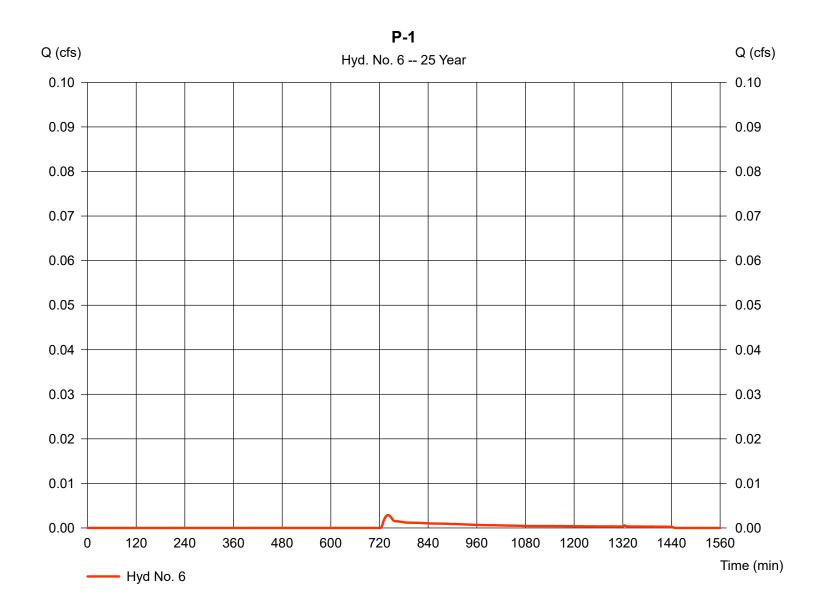
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 6

P-1

Hydrograph type = SCS Runoff Peak discharge = 0.003 cfsStorm frequency Time to peak = 741 min = 25 yrs Time interval = 1 min Hyd. volume = 29 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 5.77 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

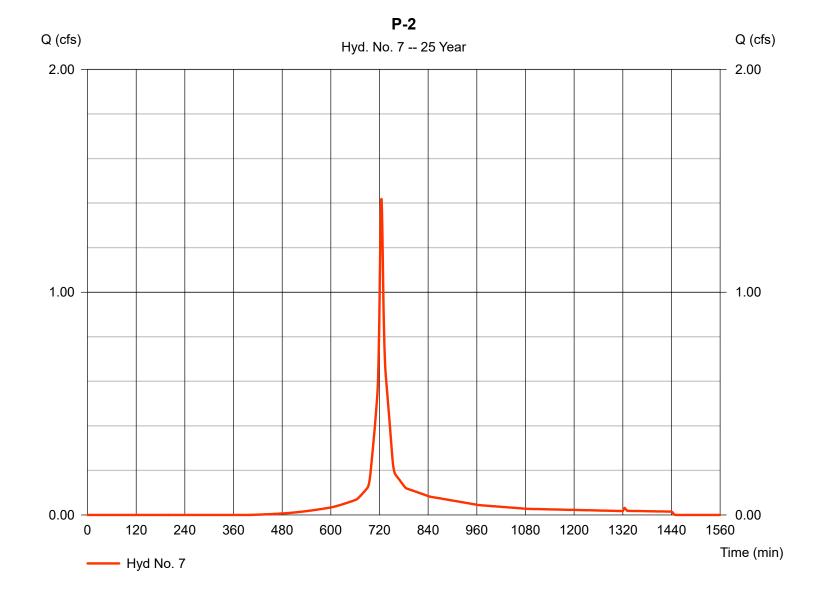
Thursday, Apr 6, 2023

Hyd. No. 7

P-2

Hydrograph type = SCS Runoff Storm frequency = 25 yrs Time interval = 1 min Drainage area = 0.320 acBasin Slope = 0.0 % Tc method = USER Total precip. = 5.77 inStorm duration = 24 hrs

Peak discharge = 1.418 cfsTime to peak $= 725 \, \text{min}$ Hyd. volume = 4,402 cuftCurve number = 81 Hydraulic length = 0 ftTime of conc. (Tc) $= 6.00 \, \text{min}$ Distribution = Type III = 484 Shape factor



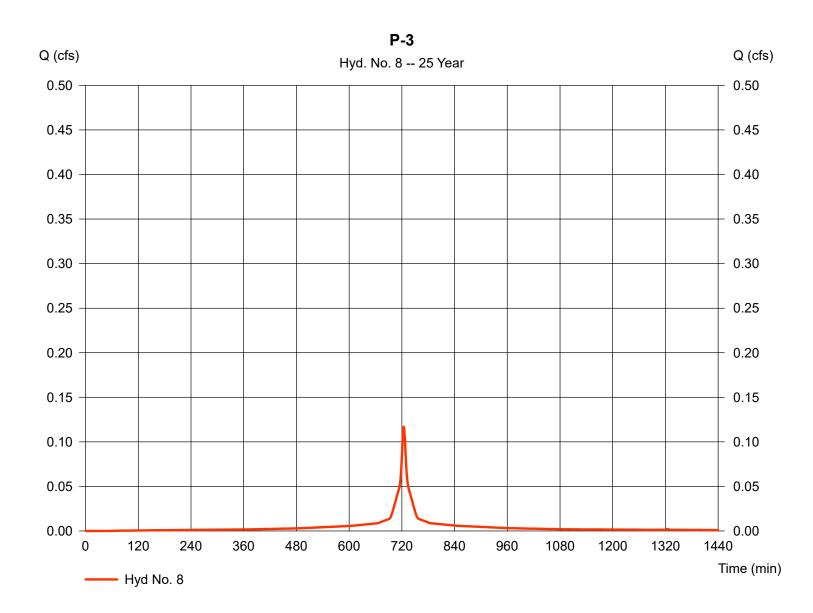
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 8

P-3

Hydrograph type = SCS Runoff = 0.117 cfsPeak discharge Storm frequency Time to peak = 724 min = 25 yrs Time interval = 1 min Hyd. volume = 414 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 5.77 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

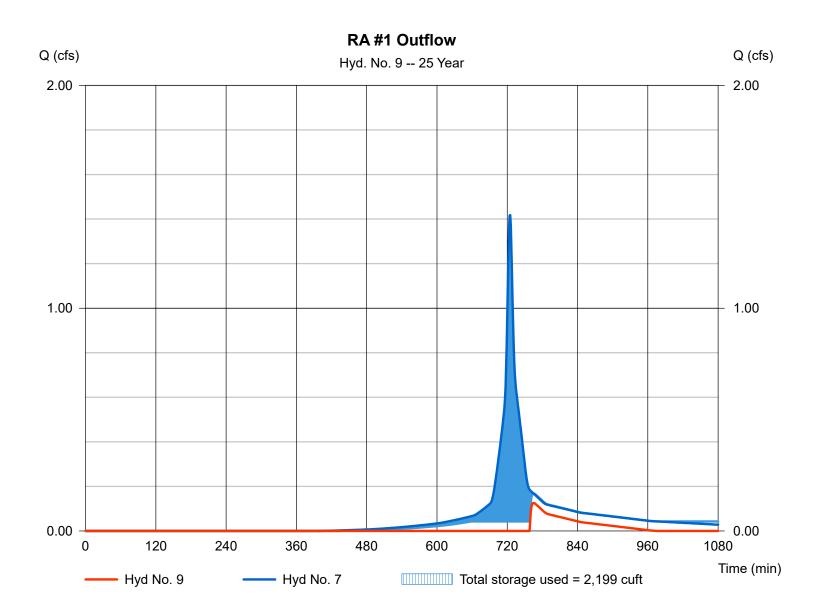
Thursday, Apr 6, 2023

Hyd. No. 9

RA#1 Outflow

Hydrograph type = Reservoir Peak discharge = 0.126 cfsStorm frequency Time to peak = 25 yrs $= 765 \, \text{min}$ Time interval = 1 min Hyd. volume = 531 cuft Inflow hyd. No. = 7 - P-2Max. Elevation = 123.27 ftReservoir name = RA #1 Max. Storage = 2,199 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



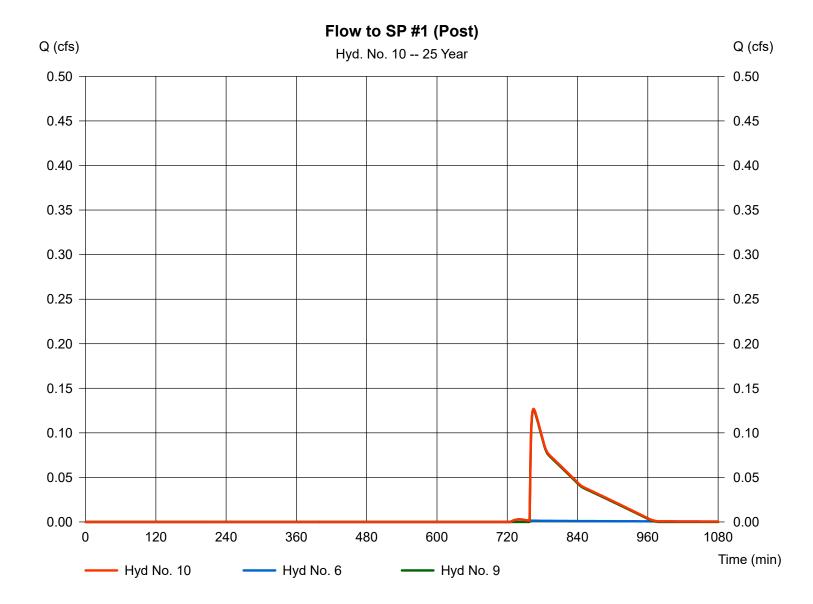
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 10

Flow to SP #1 (Post)

Hydrograph type = Combine Storm frequency = 25 yrs Time interval = 1 min Inflow hyds. = 6, 9 Peak discharge = 0.127 cfs
Time to peak = 765 min
Hyd. volume = 559 cuft
Contrib. drain. area = 0.020 ac



					Hydrallow Hydrographs by Intells				
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
1	SCS Runoff	0.006	1	730	47				E-1
2	SCS Runoff	2.089	1	724	7,057				E-2
3	SCS Runoff	0.134	1	724	476				E-3
4	Reservoir	2.081	1	724	6,748	2	123.79	206	Ex. DW outflow
5	Combine	2.223	1	724	7,533	2, 3,			Flow to SP #1 (Pre)
6	SCS Runoff	0.006	1	730	47				P-1
7	SCS Runoff	1.701	1	725	5,312				P-2
8	SCS Runoff	0.134	1	724	476				P-3
9	Reservoir	0.829	1	738	1,260	7	123.35	2,222	RA #1 Outflow
10	Combine	0.835	1	738	1,307	6, 9			Flow to SP #1 (Post)
HYI	DRO.gpw				Return F	Period: 100	Year	Thursday, A	 Apr 6, 2023

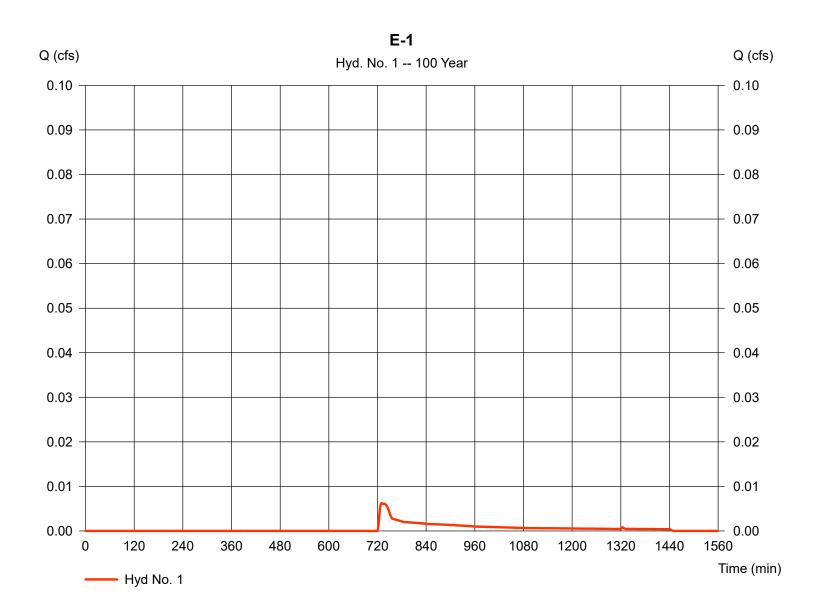
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 1

E-1

Hydrograph type = SCS Runoff Peak discharge = 0.006 cfsStorm frequency Time to peak = 100 yrs= 730 min Time interval = 1 min Hyd. volume = 47 cuft Drainage area = 0.020 acCurve number = 39 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 6.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



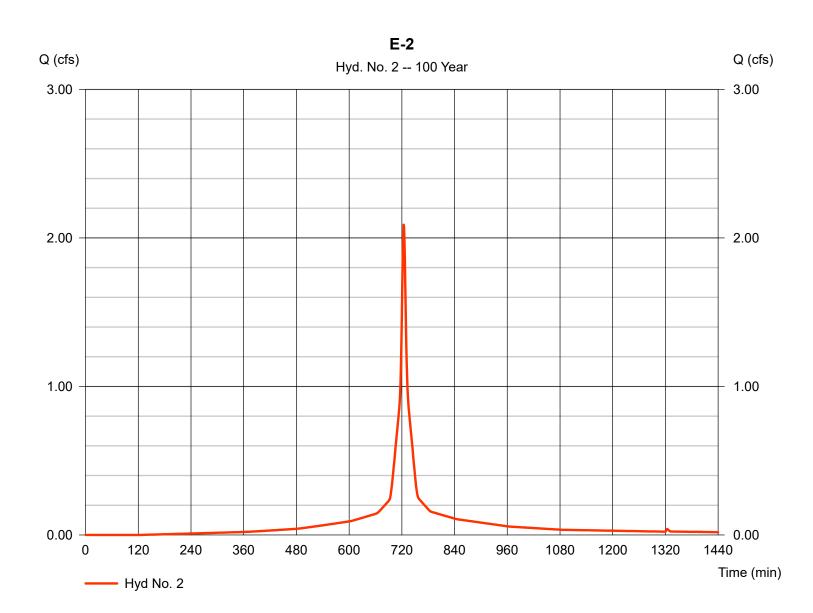
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 2

E-2

Hydrograph type = SCS Runoff = 2.089 cfsPeak discharge Storm frequency Time to peak = 724 min = 100 yrsTime interval = 1 min Hyd. volume = 7,057 cuftDrainage area = 0.320 acCurve number = 94 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 6.60 in= Type III Storm duration = 24 hrs = 484 Shape factor



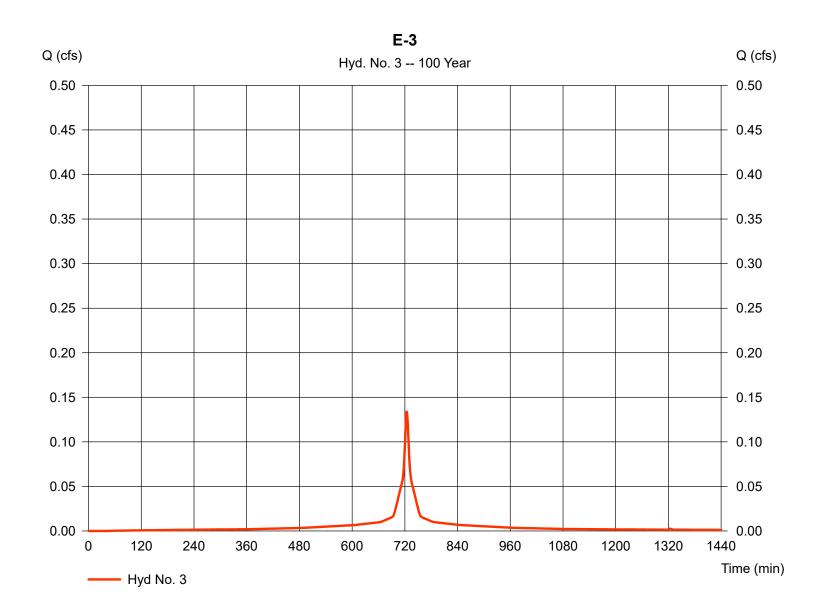
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 3

E-3

Hydrograph type = SCS Runoff Peak discharge = 0.134 cfsStorm frequency Time to peak = 724 min = 100 yrsTime interval = 1 min Hyd. volume = 476 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 6.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

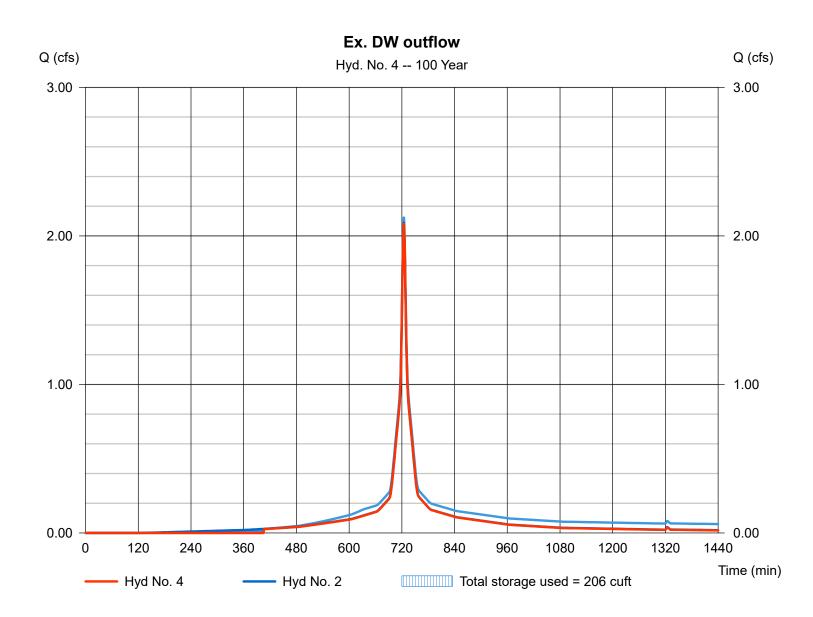
Thursday, Apr 6, 2023

Hyd. No. 4

Ex. DW outflow

Hydrograph type = 2.081 cfs= Reservoir Peak discharge Storm frequency Time to peak = 724 min = 100 yrsTime interval = 1 min Hyd. volume = 6,748 cuftInflow hyd. No. = 2 - E - 2Max. Elevation = 123.79 ftReservoir name = Ex. Drywell Max. Storage = 206 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



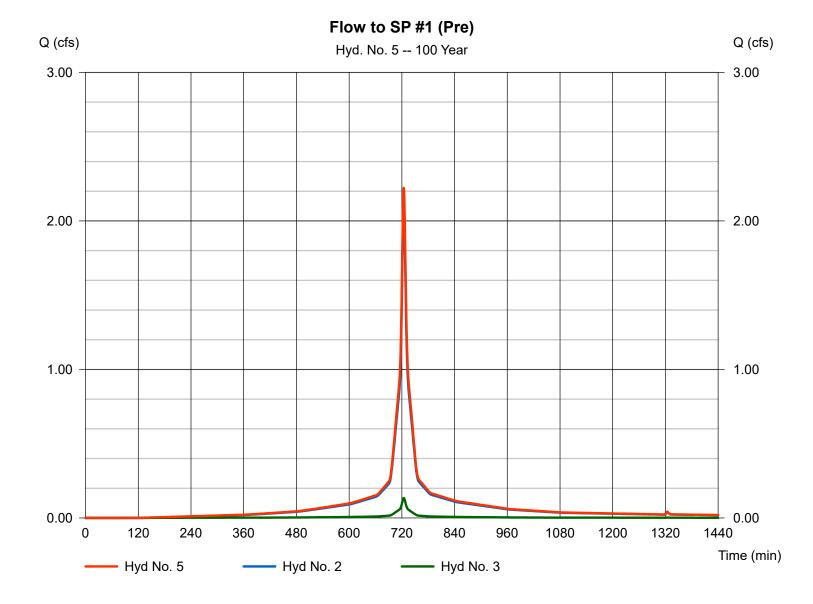
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 5

Flow to SP #1 (Pre)

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 2, 3 Peak discharge = 2.223 cfs
Time to peak = 724 min
Hyd. volume = 7,533 cuft
Contrib. drain. area = 0.340 ac



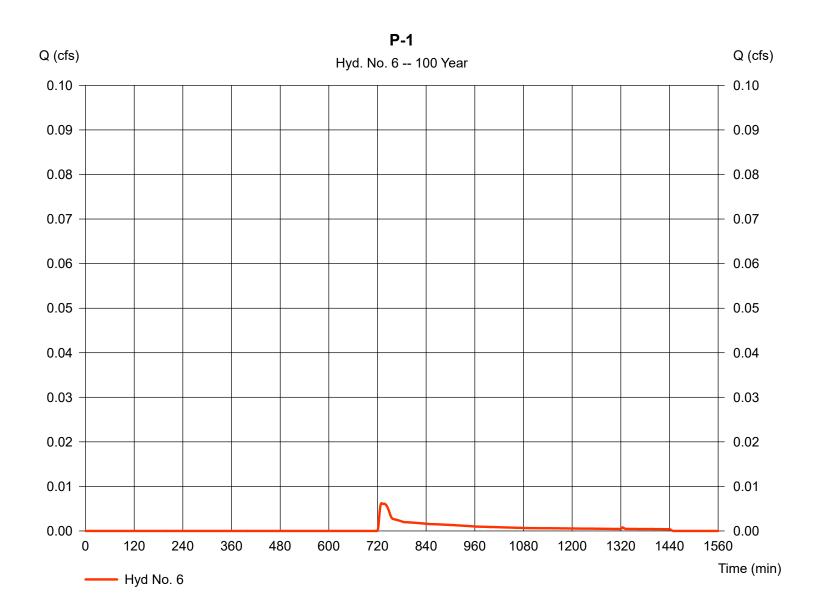
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 6

P-1

Hydrograph type = SCS Runoff Peak discharge = 0.006 cfsStorm frequency Time to peak = 100 yrs= 730 min Time interval = 1 min Hyd. volume = 47 cuft Drainage area = 0.020 acCurve number = 39Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 6.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

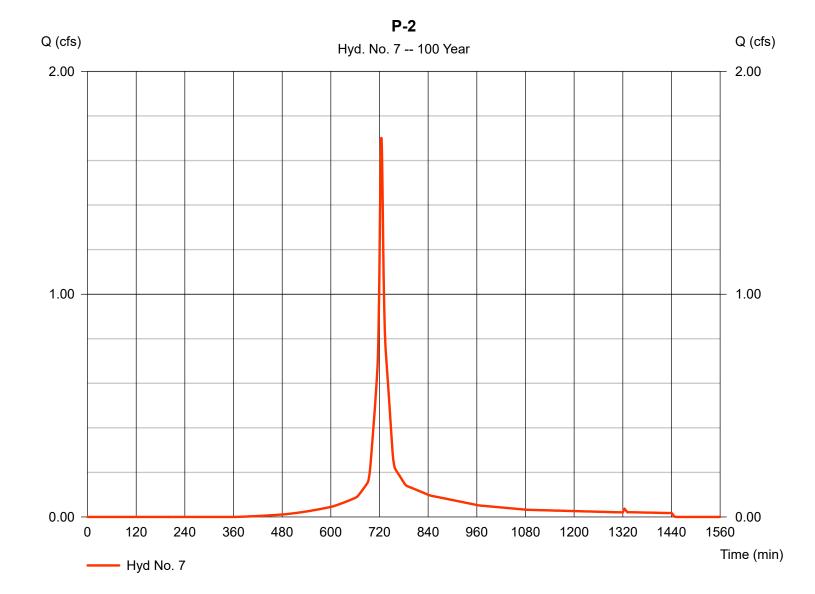
Thursday, Apr 6, 2023

Hyd. No. 7

P-2

Hydrograph type = SCS Runoff Storm frequency = 100 yrsTime interval = 1 min Drainage area = 0.320 acBasin Slope = 0.0 % Tc method = USER Total precip. = 6.60 inStorm duration = 24 hrs

= 1.701 cfsPeak discharge Time to peak = 725 min Hyd. volume = 5,312 cuftCurve number = 81 Hydraulic length = 0 ftTime of conc. (Tc) $= 6.00 \, \text{min}$ Distribution = Type III = 484 Shape factor



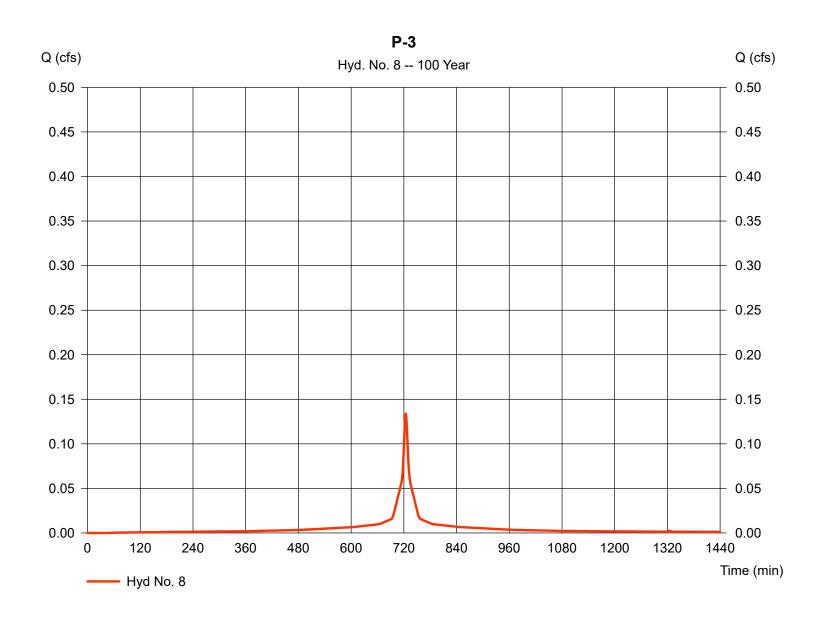
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 8

P-3

Hydrograph type = SCS Runoff Peak discharge = 0.134 cfsStorm frequency Time to peak = 724 min = 100 yrsTime interval = 1 min Hyd. volume = 476 cuft Drainage area = 0.020 acCurve number = 98 Basin Slope = 0.0 % Hydraulic length = 0 ftTc method = USER Time of conc. (Tc) $= 6.00 \, \text{min}$ Distribution Total precip. = 6.60 in= Type III Storm duration = 484 = 24 hrs Shape factor



Hydraflow Hydrographs by Intelisolve v9.2

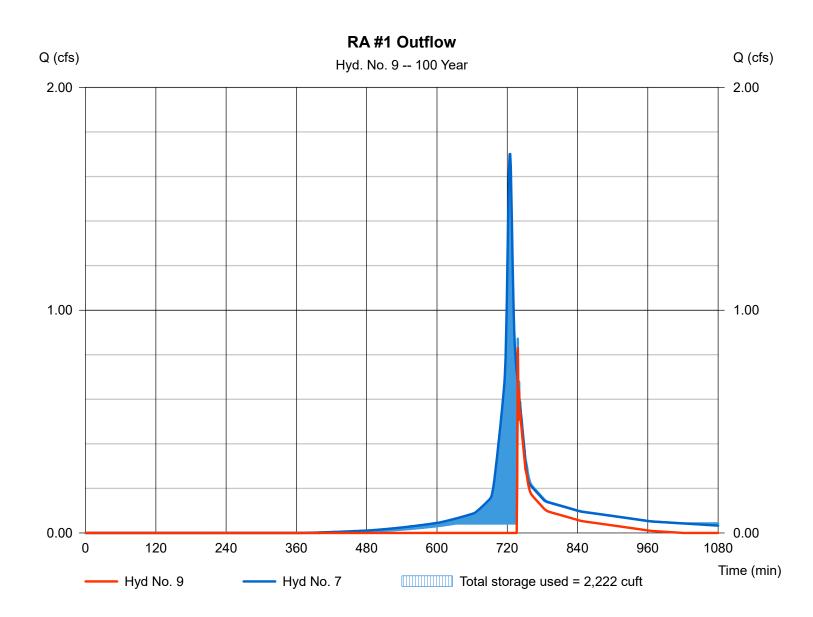
Thursday, Apr 6, 2023

Hyd. No. 9

RA#1 Outflow

Hydrograph type = Reservoir Peak discharge = 0.829 cfsStorm frequency Time to peak = 100 yrs= 738 min Time interval = 1 min Hyd. volume = 1,260 cuftInflow hyd. No. = 7 - P-2Max. Elevation $= 123.35 \, ft$ Reservoir name = RA #1Max. Storage = 2,222 cuft

Storage Indication method used. Exfiltration extracted from Outflow.



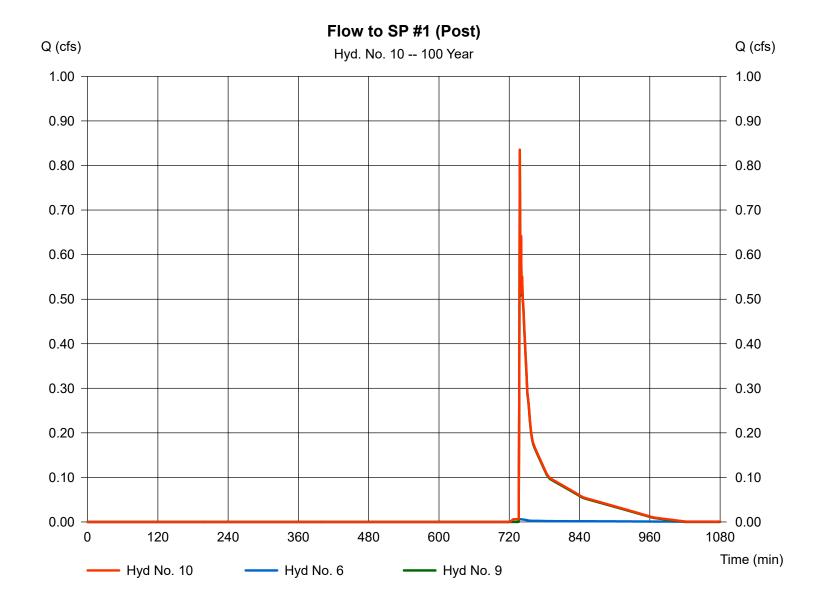
Hydraflow Hydrographs by Intelisolve v9.2

Thursday, Apr 6, 2023

Hyd. No. 10

Flow to SP #1 (Post)

Hydrograph type = Combine Storm frequency = 100 yrs Time interval = 1 min Inflow hyds. = 6, 9 Peak discharge = 0.835 cfs
Time to peak = 738 min
Hyd. volume = 1,307 cuft
Contrib. drain. area = 0.020 ac



APPENDIX 2 Standard 3 (Recharge)

Marchionda & Associates, LP 62 Montvale Ave, Suite I Stoneham, MA 02180 781-438-6121 Fax 781-438-9654

JOB 1014-01-1	90WASHINGTON ST.
SHEET NO.	- OF 1/12/29
CALCULATED BY	DATE 4/16/23
CHECKED BY	DATE

\$CALE
STANDARD #3
LOSS OF ANNUAL RECHARGE COLCULATION
PROPOSED IMPERVIOUS COVER = 10,600 SE HYDROLOGIC SOIL GROUP = "A" TARGET DEPTH = 0.60" (MA DIEIR)
HYDROLOGIC SOIL GROUP = "A"
TARGET DEPTH = 0.60" (MA DEIP)
10,600 × 0,60 1/2 = 530 FT3
VOLUME PROVIDED = 1,963 (EECHARGE)
1,963=13 >530 PF3 # STANDARD/
DRAWN DOWN COLCULATION
RECHARGE SISTEM
SOIL INFILTRATION PATE = 2.41 MAR (TABLES
TIME = (2.41 11/4R)(1=1/2")(22.3'x88') LAND)
= 11.5 HRS < 72 HRS : OKV

Pond No. 2 - RA #1

Pond Data

UG Chambers - Invert elev. = 119.00 ft, Rise x Span = 2.50 x 4.33 ft, Barrel Len = 36.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = No **Encasement** - Invert elev. = 118.50 ft, Width = 5.33 ft, Height = 4.00 ft, Voids = 40.00%

Contours - User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 122.60 ft

Stage / Storage Table

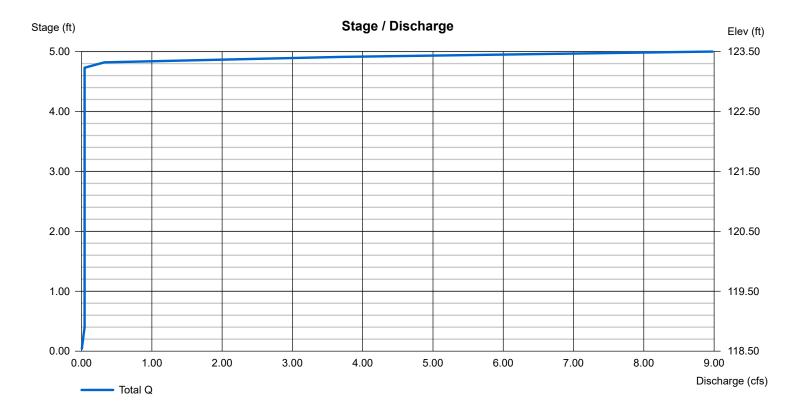
Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	118.50	n/a	0	0
0.40	118.90	n/a	123	123
0.80	119.30	n/a	235	358
1.20	119.70	n/a	269	627
1.60	120.10	n/a	262	889
2.00	120.50	n/a	250	1,140
2.40	120.90	n/a	232	1,372
2.80	121.30	n/a	203	1,575
3.20	121.70	n/a	143	1,717
3.60	122.10	n/a	123	1,840
4.00	122.50	n/a	123	1,963
4.10	122.60	50	2	1,965
5.00	123.50	800	315	2,280

Culvert / Orifice Structures

Weir Structures

	[A]	[B]	[C]	[PrfRsr]		[A]	[B]	[C]	[D]
Rise (in)	= 0.00	0.00	0.00	0.00	Crest Len (ft)	= 30.00	0.00	0.00	0.00
Span (in)	= 0.00	0.00	0.00	0.00	Crest El. (ft)	= 123.30	0.00	0.00	0.00
No. Barrels	= 0	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	0.00	Weir Type	= Rect			
Length (ft)	= 0.00	0.00	0.00	0.00	Multi-Stage	= No	No	No	No
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	= 0.60	0.60	0.60	0.60	Exfil.(in/hr)	= 2.410 (by	Contour)		
Multi-Stage	= n/a	No	No	No	TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



APPENDIX 3 Standard 4 (TSS)

	E Remaining Load (C-D)	9±10	0 2				85%
Д	D Amount Removed (BxC)	0.26	0,60				0.85
NGTON ST. WESTWOOD	C Starting TSS Load*	1.00*	0.75				Total TSS Removal =
And and a second	B TSS Removal Rate	25%	80%				Total TSS
on: 190 WASH	ABMP	DEEP SUMP DATCH BASIN	INFICTER-TION OHAM SERVE		(5)		
Calculation Worksheet							
Ā	ISVom9A 22T						

* Equals remaining load from previous BMP (E) which enters the BMP

DEP Stormwater Management Workshop

Date:

Project: 190 WASHINGTON Prepared By: T.B.

APPENDIX 4 Operation & Maintenance Plan

OPERATION AND MAINTENANCE

&

LONG TERM POLLUTION PREVENTION PLAN FOR POST-CONSTRUCTION STORM WATER CONTROLS

190 WASHINGTON STREET WESTWOOD, MASSACHUSETTS

April 12, 2023

GENERAL

The Best Management Practices (BMPs) used in the design of the 190 Washington Street project were chosen for their effectiveness at reducing peak discharge and infiltrating groundwater. Routine maintenance is required for the BMPs, as proper maintenance is essential in achieving the desired result of improved water quality. This Operations and Maintenance (O&M) and Long Term Pollution Prevention Plan (LTPPP) is intended to cover the post-construction maintenance of the permanent BMPs¹ and site specific pollution prevention.

MAINTENANCE REQUIREMENTS

Qualified personnel shall inspect all components of the stormwater management system as outlined below. To be considered "qualified", personnel should have a working knowledge of the maintenance requirements of storm water BMP's and must be approved by the Westwood DPW. Qualified personnel shall be responsible for overseeing the required inspections and shall file annual reports with the town of Lawrence officials. Additionally, a copy of the Inspection/Maintenance Log, as further described herein, shall be provided to town of Lawrence officials on an annual basis.

SUMMARY OF MAINTENANCE REQUIREMENTS

BMP	MIN. FREQUENCY	RESPONSIBLE PARTY
Drive and Parking Area	once/quarter	Skye Realty Management,
Sweeping		LLC
Trash Removal	Inspect once/month	Skye Realty Management,
	Clean as necessary	LLC
Catch Basin	Inspect 4x/year	Skye Realty Management,
	Clean once/year	LLC
Infiltration Chambers	Inspect Once/year	Skye Realty Management,
	Maintain as necessary	LLC

¹ Operations and maintenance of temporary erosion and sedimentation controls utilized during construction will be covered by a *Stormwater Pollution Prevention Plan* as required by the National Pollutant Discharge Elimination System program of the Environmental Protection Agency, and is not part of this O&M Plan.

April 12, 2023

RESPONSIBILITY TO ADMINISTER O&M PLAN

During construction, the general contractor will be responsible for maintaining the stormwater management system in accordance with this O&M Plan until such time that ownership of the project or phases thereof are turned over to the owner. The owner is then responsible for maintaining the portions of the stormwater management system under their ownership in accordance with this O&M Plan. This section below (names and signatures) shall be updated with every change in ownership and/or person(s) responsible for administering/financing the O&M of the system.

Owner(s) of the stormwater management	system:
Name:	Name:
Signature:	Signature:
Person(s) responsible for financing maint	tenance and emergency repairs:

INSPECTION AND MAINTENANCE LOG

A sample inspection and maintenance log to be used is attached to the end of this O&M Plan. At a minimum, any inspection and maintenance log used shall include the following items:

- Date activity performed
- Specific inspection/maintenance task
- Structural components inspected/maintained
- Staff person or contractor performing activity
- Supervisor verification of maintenance activity
- Recommended additional maintenance tasks

An Annual Report shall be submitted to the Town of Westwood to meet the requirements of the town's Stormwater Management and Erosion Control Regulations.

April 12, 2023

PROPOSED BMPS AND CORRESPONDING O&M REQUIREMENTS:

DRIVEWAY and PARKING AREA SWEEPING:

Sweeping of impervious surfaces shall be conducted once per quarter. All sweepings shall be handled and disposed of in accordance with applicable local, state and federal guidelines and regulations.

TRASH REMOVAL:

The field areas shall be inspected for litter and trash monthly as part of overall site maintenance. Any accumulated trash, litter and discarded materials in these areas shall be removed.

No disposal of materials will be permitted within the landscaped areas or wooded areas on the Site. This prohibition applies to trash, fill material, construction debris, grass clippings, collected leaves and cut branches.

CATCH BASIN:

The catch basin shall be inspected four times per year for build-up of sediment, oil, and/or other debris which could decrease the effectiveness of the sumps. A qualified company specializing in the cleaning of catch basins shall perform the inspection of catch basins.

Typically a dipstick tube equipped with a ball valve, such as a Sludge Judge[®], is used to measure the approximate oil and sediment depth, and a vacuum truck is used to clean out the catch basin. Catch basins shall be cleaned once per year, or sooner if the depth of sediment is found to reach 12 inches. If visual inspection observes any evidence of hydrocarbons, the material shall be immediately cleaned and disposed in accordance with all applicable local, state and federal guidelines and regulations.

As part of the inspection, catch basins should be inspected for structural soundness. Hoods and associated hardware should be inspected to ensure that they are correctly attached and functioning properly. Catch basins shall be repaired or replaced as necessary to ensure proper operation.

Frames and grates should be inspected and repaired or replaced as necessary to ensure proper operation.

Budget for Catch Basin Inspections and Maintenance: \$1,000/year

April 12, 2023

INFILTRATION CHAMBERS:

The project includes a roof drainage recharge system comprised of 15 HDPE infiltration chambers. The system includes clean out junction manholes and observation ports located in the chambers.

It is important to occasionally inspect the system to ensure that it remains clear of any debris and sediment. This will help to ensure that trenches will continue to function efficiently long term.

To accomplish this, the system should be inspected once every year. A stadia rod should be used to measure the depth of sediment in the chambers. Should the depth of sediment exceed six inches the basin(s) should be cleaned of the sediment. In the event that the system would need to be cleaned, a culvert cleaning nozzle such as a JetVac® is recommended.

Budget for Chamber Inspections and Maintenance: \$1,000/year

LONG TERM POLLUTION PREVENTION:

MAINTENANCE OF LANDSCAPED AREAS:

Fertilizers used for landscaping and lawn areas shall be slow release, low-nitrogen types (<5%) and shall not be used within 25 feet of a wetland resource area, and pesticides/herbicides shall not be used within 100 feet of a wetland resource area. Furthermore, the use of any fertilizers, pesticides, and herbicides shall be in accordance with the manufacturer's recommendations.

WINTER MAINTENANCE OF WALKS AND DRIVES:

Snow storage shall take place on pervious surfaces to the extent practicable to allow the snowmelt to filter through the soil, leaving behind sand and debris that can be removed in the springtime. Snow shall not be stockpiled in drainage collection areas or conveyance channels as this may block the system causing flooding. Furthermore, snow shall not be stored in or within 25 feet of a wetland resource area. No road salt, sodium chloride, or other deicing chemicals shall be used on paved surfaces within 25 feet of a wetland resource area.

April 12, 2023

STORAGE OF WASTE PRODUCTS:

Any outdoor storage of waste products shall be covered to prevent rainfall from picking up contaminants from the waste. This requirement shall include any dumpster(s) which shall have the lid(s) closed when not being loaded or unloaded.

ILLICIT DISCHARGES:

There shall be no illicit discharges to the stormwater management system. Illicit discharges are defined by 310 CMR 10.04 as follows:

"Illicit discharge means a discharge that is not entirely comprised of stormwater. Notwithstanding the foregoing, an illicit discharge does not include discharges from the following activities or facilities: firefighting, water line flushing, landscape irrigation, uncontaminated ground water, potable water sources, foundation drains, air conditioning condensation, footing drains, individual resident car washing, flows from riparian habitats and wetlands, dechlorinated water from swimming pools, water used for street washing and water used to clean residential buildings without detergents."

Prior to the discharge of stormwater runoff to the post-construction stormwater best management practices, an Illicit Discharge Compliance Statement shall be submitted to the Lawrence Planning Board verifying that no illicit discharges exist on the site.

EMERGENCY SPILLS

The owner shall provide personnel with a list of emergency contact phone numbers to use to report a spill. At a minimum the list should include the DEP Emergency Response Section, an environmental cleanup contractor such as Clean Harbors, Inc., the Lawrence Fire Department, and a contact person/phone number for the owner:

DEP Emergency Response
 Clean Harbors, Inc.
 1(888)304-1133
 1(800)645-8265

- Westwood Fire Department 911 or (781)-320-1000
- Owner (*Skye Realty Management, LLC*)

While the above-listed phone numbers are current as of the writing of this O&M Plan, the owner shall be responsible for verifying these numbers prior to distribution to the homeowners. Additionally, the owner shall update and redistribute a list of emergency contact phone numbers to the homeowners every other year, or sooner should any changes occur.